

Appendix 3

Properties of Biomass¹

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PROPERTIES OF BIOMASS RELEVANT TO GASIFICATION

An understanding of the structure and properties of biomass materials is necessary to evaluate their utility as feedstocks for conversion processes. This section summarizes available information on a variety of such properties including chemical analysis, heats of combustion and formation, physical structure, heat capacities, and transport properties of biomass feedstocks and chars. Much of the information reported is for wood materials; however, where data were available for other forms of biomass such as municipal solid waste and feedlot waste, they were included.

3.1 BULK CHEMICAL ANALYSIS OF BIOMASS

In evaluating gasification feedstocks, it is generally useful to have proximate and ultimate analyses, heats of combustion, and sometimes ash analyses. These provide information on volatility of the feedstock, elemental analysis, and heat content. The elemental analysis is particularly important in evaluating the feedstock in terms of potential pollution.

Table 3-1 lists the standard Methods for evaluating carbonaceous feedstocks.

A number of instruments have been developed for determining elemental composition, most often, in biomass conversion, for carbon, hydrogen, nitrogen, sulfur, and oxygen. Chlorine normally is not determined by such analyzers. Most of these systems employ a catalytic combustion or pyrolysis step to decompose the sample to carbon dioxide, water, hydrogen sulfide, and nitrogen, which are then determined quantitatively by as chromatography using flame ionization (FID) or thermal conductivity (TC) detectors. Oxygen is usually determined by catalytic conversion to carbon monoxide over a platinized carbon catalyst followed by GC analysis. A short list of some representative equipment is given in Table 3-2.

3.1.1 Proximate Analyses

The proximate analysis classifies the fuel in terms of its moisture (M), volatile matter (VM), ash, and (by difference) fixed carbon content. In the test procedure, the volatile material is driven off in an inert atmosphere at high temperatures (950°C) using a slow heating rate. The pyrolysis yield is representative of that for slow pyrolysis processes; fast pyrolysis techniques employing very rapid heating rates normally yield more volatile matter. The moisture determined by the proximate method represents physically bound water only; water released by chemical reactions during pyrolysis is classified with the volatiles. The ash content is determined by combustion of the volatile and fixed carbon fractions. The resulting ash fraction is not representative of the original ash, more appropriately termed mineral matter, due to the oxidation process employed in its determination. In the most exact analysis, small corrections to the ash weight are necessary to correct it to a mineral

Table 3-1: ASTM Standards Methods for Biomass and Coal

Method	Biomass Test No.	Coal Test No.	Repeatability (wt%)	Reproducibility (wt%)
Proximate Analysis				
Moisture	E871	D2013, D3173	0.5	1.0
Volatile Matter	E872, E897	D3175	0.5	1.0
Ash	D1102, E830	D3174	0.6	1.3
Fixed Carbon	Difference	Difference		
Ultimate Analysis		D3176		
C	E777	D3176	0.5	1.6
H	E777	D3178	0.2	0.5
N	E778	D3179	0.04	0.05
S	E775	D4239, D3177	0.03	0.06
O	Difference	Difference		
Chlorine	E776	D2361	0.03	0.11
Gross Heating Value	E711, D2015	D2015	27-111 Btu/lb ^c	68-250 Btu/lb ^c
Ash Analysis				
Ash in Biomass	E1755		2.7 ^d	8.9 ^d
Ash in wood	D1102		0.03 (6.6 ^d)	
Elemental Ash	D3682, D2795		5 ^d See element	
Fusion temp	D1857		50°F	
Water soluble alkali	Soak overnight in H ₂ O @90 C, Analyze by AA			
Bulk Density	E873		TBD	TBD
Fuel size (based on RDF)	E828			

^a within laboratory; ^b between laboratories; ^c dependent on magnitude of HHV

^d % of average

matter basis. The fixed-carbon content of an as received sample is calculated by material balance. Thus:

$$FC = 1 - M - ASH - VM \quad (3-1)$$

The fixed carbon is considered to be a polynuclear aromatic hydrocarbon residue resulting from condensation reactions which occur in the pyrolysis step.

Table 3-2: Elemental Analyzer Equipment

Instrument	Oxidant	Capability	Detection
Carlo Erba 1104	oxygen	C, H, N, O	FID & TIC
Chemical Data Systems (CDS 1200)	oxygen	C, H, N, O, S and functional groups	FID & TC
Hewlett-Packard HP-185	MNO ₂ added	C, H, N	FID & TC
Perkin Elmer 240	oxygen	C, H, N, O, S	TC

The most useful basis for reporting proximate analysis is the dry basis. In this instance the compositions are normalized to a moisture-free basis (denoted by *):

$$VM^* + FC^* + ASH = 1, \quad (3-2)$$

and, for example,

$$VM^* = VM/(1-M).$$

The moisture is reported as grams of moisture per gram of dry feedstock. Typical proximate analyses for solid fuels are given in Table 3-3, from which it is evident that common biomass materials are more readily devolatilized (pyrolyzed) than lignite and bituminous coals, yielding considerably less fixed-carbon residue. This is due to the much more aromatic structure of the coals which is produced by the geological coalification process. The higher volatile content of biomass materials makes them potentially useful feedstocks for pyrolysis processes. In general, the ash content of biomass materials is considerably lower than for coals. This is due to the fact that the bulk of the coal ash was deposited in coal beds by processes such as siltation and did not come from the parent carbonaceous material. An exception is municipal solid waste, which contains a high mineral content due to nonvolatile trash components such as metals and glass.

Table 3-3: Proximate Analysis Data for Selected Solid Fuels and Biomass
(Dry basis, wt%)

	Volatile Matter (VM)	Fixed Carbon (FC)	Ash	Reference
<u>Coals</u>				
Pittsburgh seam	33.9	55.8	10.3	Bituminous Coal Research 1974
Wyoming Elkol	44.4	51.4	4.2	
Lignite	43.0	46.6	10.4	
<u>Oven Dry Woods</u>				
Western hemlock	84.8	15.0	0.2	Howlett and Gamanche 1977
Douglas fir	86.2	13.7	0.1	
White fir	84.4	15.1	0.5	
Ponderosa pine	87.0	12.8	0.2	
Redwood	83.5	16.1	0.4	
Cedar	77.0	21.0	2.0	
<u>Oven Dry Barks</u>				
Western hemlock	74.3	24.0	1.7	Howlett and Gamance 1977
Douglas fir	70.6	27.2	2.2	
White fir	73.4	24.0	2.6	
Ponderosa pine	73.4	25.9	0.7	
Redwood	71.3	27.9	0.8	
Cedar	86.7	13.1	0.2	
<u>Municipal Refuse and Major Components</u>				
Nat'l Ave. Waste	65.9	9.1	25.0	Klass and Ghosh 1973
Newspaper (9.4%)	86.3	12.2	1.5	
Paper boxes (23.4%)	81.7	12.9	5.4	
Magazine paper (6.8%)	69.2	7.3	23.4	
Brown paper (5.6%)	89.1	9.8	1.1	
<u>Selected Biomass</u>				
Almond wood	77.28	15.94	6.78	Miles et. al. 1995
Red oak sawdust	86.22	13.47	0.31	
Hybrid poplar	84.81	12.49	2.70	
Alfalfa stems	78.92	15.81	5.27	
Wheat straw, Denmark	69.80	12.29	10.78	
Wheat straw, OR	81.24	17.06	4.32	
Rice straw	65.47	15.86	18.67	
Willow	85.23	13.82	0.95	
Sugar cane bagasse	85.61	11.95	2.44	
Switchgrass, MN	82.94	14.37	2.69	
Bana Grass	73.44	16.68	9.88	

3.1.2 Ultimate Analyses

Ultimate analyses generally report C, H, N, S and O (by difference) in the solid fuel. Table 3-1 lists the appropriate ASTM tests for these elements while Table 3-2 lists several manufacturers of modern elemental analyzers. Care must be exercised in using ultimate analyses for fuels containing high moisture content because moisture is indicated in the ultimate analysis as additional hydrogen and oxygen.

To avoid confusion and give a good representation of the fuel itself, ultimate analyses should be performed and reported on a dry basis; when this is done all hydrogen determined is truly a constituent of the fuel. For certain biomass materials like municipal solids and animal waste, the determination of chlorine is important because it represents a possible pollutant and corrosive agent in gasification and combustion systems.

Typical ultimate analyses for a variety of feedstocks are presented in Table 3-4.

All biomass materials have carbon contents considerably lower than coals; the atomic carbon to hydrogen ratio is much higher in coals than in biomass materials. For coal, the H/C ratio is unity, while for biomass the ratio is typically 1.5. The bound oxygen content of biomass materials is considerably higher, due to the ether, acid, and alcohol groups in the cellulose, hemicellulose, and lignin fractions of biomass, as will be discussed later in this section. The nitrogen and sulfur contents in coal are considerably higher than those in most biomass. Thus, in direct biomass combustion, pollutants resulting from bound nitrogen and sulfur in the fuel generally are present in small enough quantities to meet EPA standards, although the high chlorine contents that are found in animal wastes can pose a severe pollution problem. The nitrogen content, normalized by heating value, of selected samples from Table 3-4 is given in Figure 3-1. Alkali content of biomass is important also because of its potential impact on slagging and fouling in combustion and gasification systems. A recent study (Miles 1995) found that biomass feeds containing less than 0.5 lb K per million Btu did not cause fouling and slagging in commercial biomass boilers. The potassium content of selected biomass samples from Table 3-4 is shown in Figure 3-2.

The relative “quality” of the volatile matter can be estimated using the ultimate analysis and simple stoichiometry. If it is assumed that the fixed carbon contains only carbon, then all hydrogen and oxygen plus a portion of the carbon are associated with the volatile materials. Table 3-5 presents a typical calculation for the volatile fraction of lignite and Douglas fir bark.

Table 3-4: Ultimate Analysis Data for Selected Solid Fuels and Biomass Materials
(Dry basis, wt %)

Material	C	H	N	S	O	Cl	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Pittsburgh seam coal	75.5	5.0	1.2	3.1	4.9	--	10.3	13,650	31.68	Tillman 1978
West Kentucky No. 11 coal	74.4	5.1	1.5	3.8	7.9	--	7.3	13,460	31.24	Bituminous Coal Research 1974
Utah coal	77.9	6.0	1.5	0.6	9.9	--	4.1	14,170	32.89	Tillman 1978
Wyoming Elkol coal	71.5	5.3	1.2	0.9	16.9	--	4.2	12,710	29.50	Bituminous Coal Research 1974
Lignite	64.0	4.2	0.9	1.3	19.2	--	10.4	10,712	24.86	Bituminous Coal Research 1974
Charcoal	80.3	3.1	0.2	0.0	11.3	--	3.4	13,370	31.03	Tillman 1978
Alder, red	49.55	6.06	0.13	0.07	43.78		0.40	8,578	19.91	Rossi
Alder/fir sawdust	51.02	5.80	0.46	0.05	68.54	0.02	4.13	8,760	20.33	Miles et. al. 1995
Alfalfa Pellets	44.90	5.60	2.90	0.22	37.08	0.39	9.30	7,807	18.12	MN Project
Alfalfa Pellets	45.60	5.50	2.70	0.21	36.99	0.39	9.00	7,880	18.29	MN Project
Alfalfa seed straw	46.76	5.40	1.00	0.02	40.72		7.25	7,949	18.45	Jenkins and Ebeling
Almond hulls	45.79	5.36	0.96	0.01	40.60		5.78	7,850	18.22	Jenkins and Ebeling
Almond prunings	51.30	5.29	0.66	0.01	40.90		1.63	8,621	20.01	Jenkins and Ebeling
Almond shells	44.98	5.97	1.16	0.02	42.27		4.81	8,350	19.38	Jenkins and Ebeling
Almond wood	47.45	5.53	0.59	0.08	39.57	0.03	6.78	6,829	15.85	Miles et. al. 1995
Animal waste	42.7	5.5	2.4	0.3	31.3		17.8	7,380	17.13	Tillman 1978
Ash, white	49.70	6.90			43.00		0.30	8,940	20.75	Johnson and Auth
Bagasse	39.70	5.50	0.30		42.30		13.30	6,756	15.68	Mudge et al
Bagasse	44.80	5.35	0.38	0.01	39.55		11.27	7,467	17.33	Jenkins and Ebeling
Bagasse	46.27	5.27	0.12	0.05	42.41	0.05	5.83	7,885	18.30	Turn et. al.
Bagasse	48.64	5.87	0.16	0.04	42.85	0.03	2.44	8,166	18.95	Miles et. al. 1995
Bagasse	45.71	5.89			40.37		8.03	8,402	19.50	Grover and Anuradha
Bana Grass, HI	45.06	5.42	0.84	0.11	38.69	0.83	9.88	7,533	17.48	Miles et. al. 1995
Banagrass	47.10	5.29	0.44	0.16	41.93	0.61	4.47	7,897	18.33	Turn et. al.
Bark	47.27	5.20	0.40	0.05	37.68	0.03	9.37	7,721	17.92	Feldman et. al.
Bean straw	42.97	5.59	0.83	0.01	44.93		5.93	7,523	17.46	Jenkins and Ebeling
Beech	51.6	6.3	0.0	0.0	41.5		0.6	8,760	20.33	Tillman 1978
Birch and maple mix	49.86	6.12	0.10	0.09	43.45	0.03	0.36	8,453	19.62	Feldman et. al.
Birch, white	49.80	6.50			43.40		0.30	8,669	20.12	Johnson and Auth

Material	C	H	N	S	O	Cl	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Black locust	50.73	5.71	0.57	0.01	41.93		0.80	8,492	19.71	Jenkins and Ebeling
Black walnut prunings	49.80	5.82	0.22	0.01	43.25		0.78	8,544	19.83	Jenkins and Ebeling
Cabernet Sauvignon prunings	46.59	5.85	0.83	0.04	43.90		2.17	8,199	19.03	Jenkins and Ebeling
Casuarina	48.50	6.04	0.31	0.00	43.32		1.83	8,087	18.77	Channiwala
Casuarina	48.61	5.83	0.59	0.02	43.36		1.40	8,376	19.44	Jenkins and Ebeling
Cedar bark	51.00	5.70			38.20		5.10	8,630	20.03	Johnson and Auth
Cedar, white	48.80	6.40			44.40		0.40	8,018	18.61	Johnson and Auth
Chaparall	46.90	5.08	0.54	0.03	40.17		6.13	8,337	19.35	Jenkins and Ebeling
Chenin Blanc prunings	48.02	5.89	0.86	0.07	41.93		2.51	8,242	19.13	Jenkins and Ebeling
Cherry	48.52	5.81	0.31	0.02	42.97	0.02	1.35	8,408	19.51	Feldman et. al.
Chinkapin	49.68	5.93	0.07	0.01	44.03		0.30	8,337	19.35	Rossi
Christmas trees	51.59	5.58	0.52	0.40	36.70	--	5.21	9,009	20.91	Miles et. al. 1995
Cocoa hulls	48.23	5.23	2.98	0.12	33.19		8.25	8,203	19.04	Jenkins and Ebeling
Coconut fiber (coir)	50.29	5.05	0.45	0.16	39.63		3.72	8,639	20.05	Channiwala
Coconut shells	50.22	5.07	0.00	0.00	43.37		0.71	8,832	20.50	Channiwala
Corn cobs	46.58	5.87	0.47	0.11	45.46		1.36	8,087	18.77	Jenkins and Ebeling
Corn stover	43.65	5.56	0.61	0.01	43.31		5.58	7,604	17.65	Jenkins and Ebeling
Corn Stover	46.50	5.81	0.56	0.11	39.67		7.40	8,186	19.00	Gregory et al
Corn stover	46.51	5.81	0.56	0.11	39.67		7.00	8,782	20.38	Evans et. al.
Cotton gin trash	39.59	5.26	2.09	2.09	36.38		17.60	7,075	16.42	Jenkins and Ebeling
Cotton gin waste	42.66	6.05	0.18		49.50		1.61	7,531	17.48	Channiwala
Cotton stalk	39.47	5.07	1.25	0.02	38.09		17.20	6,820	15.83	Channiwala
Cotton stalk	43.64	5.81	0.00	0.00	43.87		6.68	7,867	18.26	Grover and Anuradha
Cypress	55.00	6.50			38.10		0.40	9,892	22.96	Johnson and Auth
Demolition wood	46.30	5.39	0.57	0.12	34.50	0.05	13.12	7,916	18.37	Miles et. al. 1995
Douglas fir	50.64	6.18	0.06	0.02	43.00		0.10	8,837	20.51	Rossi
Douglas fir	52.3	6.3	0.1	0.0	40.5		0.8	9,050	21.01	Tillman 1978
Douglas fir bark	56.2	5.9	0.0	0.0	36.7		1.2	9,500	22.05	Tillman 1978
Elm	50.40	6.60			42.30		0.70	9,039	20.98	Johnson and Auth
Eucalyptus Camaldulensis	49.00	5.87	0.30	0.01	43.97		0.76	8,367	19.42	Jenkins and Ebeling
Eucalyptus Globulus	48.18	5.92	0.39	0.01	44.18		1.10	8,285	19.23	Jenkins and Ebeling
Eucalyptus Grandis	48.33	5.89	0.15	0.01	45.13		0.52	8,337	19.35	Jenkins and Ebeling

Material	C	H	N	S	O	Cl	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Fir mill waste	51.23	5.98	0.06	0.03	42.29	0.19	0.41	8,779	20.38	Miles et. al. 1995
Fir, white	49.00	5.98	0.05	0.01	44.75		1.52	8,367	19.42	Jenkins and Ebeling
Forest residuals	50.31	4.59	1.03	0.11	39.99	0.04	3.97	8,670	20.12	Miles et. al. 1995
Furniture waste	49.87	5.91	0.29	0.03	40.29	<0.01	3.61	8,658	20.10	Miles et. al. 1995
Grape pomice	54.94	5.83	2.09	0.21	32.08		4.20	9,393	21.80	Grover and Anuradha
Groundnut shells	48.59	5.64	0.58	0.00	39.49		5.70	8,552	19.85	Johnson and Auth
Gum	50.88	6.06	0.15	0.04	41.57	0.02	1.28	8,475	19.67	Feldman et. al.
Hardwood	49.73	6.06	0.24	0.04	42.87	0.11	0.95	8,430	19.57	Feldman et. al.
Hemlock, western	50.4	5.8	0.1	0.1	41.4		2.2	8,620	20.01	Tillman 1978
Hickory	49.7	6.5	0.0	0.0	43.1		0.7	8,670	20.12	Tillman 1978
Hog fuel	45.36	5.63	0.18	0.02	42.13	0.03	16.89	7,681	17.83	Feldman et. al.
Kelp, brown, Soquel Point	27.80	3.77	4.63	1.05	23.69		42.10	4,632	10.75	Chynoweth et al
Kelp, giant brown, Monterey	26.60	3.74	2.55	1.09	20.22		45.80	4,421	10.26	Chynoweth et al
Macadamia shells	54.41	4.99	0.36	0.01	39.69		0.40	9,052	21.01	Jenkins and Ebeling
Madrone	48.56	6.05	0.05	0.02	45.08		0.30	8,246	19.14	Rossi
Madrone	48.94	6.03	0.05	0.02	41.74		0.20	8,406	19.51	Rossi
Mango wood	46.24	6.08	0.28		44.42		2.98	8,259	19.17	Johnson and Auth
Manzanita	48.18	5.95	0.17	0.02	44.68		0.82	8,315	19.30	Jenkins and Ebeling
Maple	49.54	6.11	0.10	0.02	49.54		0.50	8,306	19.28	Evans et. al.
Maple	50.6	6.0	0.3	0.0	41.7		1.4	8,580	19.91	Tillman 1978
Millet straw	43.71	5.85	0.01	0.00	45.16		5.27	7,777	18.05	Channiwala
Mixed waste paper	47.99	6.63	0.14	0.07	36.84		8.33	8,934	20.74	Miles et. al. 1995
Mixed wood	49.31	6.03	0.18	0.02	42.98	0.04	1.44	8,366	19.42	Feldman et. al.
Mixed wood (90% red oak)	48.51	6.17	0.12	0.04	44.22		0.94	8,210	19.06	Evans et. al.
Mixed wood	48.40	6.31	0.21	0.03	44.23		0.82	8,228	19.10	Evans et. al.
Municipal solid waste	47.6	8.0	1.2	0.3	32.9		12.0	8,546	19.84	Saner et. al. 1970
Napier grass	45.20	6.00			42.30		5.70	7,889	18.31	Elliot et al
Oak	49.83	5.87	0.32	0.04	41.82	0.03	2.09	8,373	19.43	Feldman et. al.
Oak, Alabama woodwaste	49.5	5.7	0.2	0.0	41.3	--	3.3	8,266	19.19	Boley and Landers 1969
Oak, Canyon	47.84	5.80	0.07	0.01	45.76		0.50	8,178	18.98	Rossi
Oak, red	49.34	5.93	0.07	0.13	41.74	0.03	2.76	8,220	19.08	Feldman et. al.
Oak, red, sawdust	49.96	5.92	0.03	0.01	43.77	0.07	0.31	8,374	19.44	Miles et. al. 1995

Material	C	H	N	S	O	Cl	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Oak, tan	48.67	6.03	0.06	0.04	44.99		0.20	8,156	18.93	Rossi
Oak, tan	48.34	6.12	0.03	0.03	44.99		0.50	8,238	19.12	Jenkins and Ebeling
Oak, white	49.48	5.38	0.35	0.01	43.13		1.52	8,367	19.42	Jenkins and Ebeling
Olive pits	48.81	6.23	0.36	0.01	43.48		3.20	9,216	21.39	Channiwala
Paper	43.4	5.8	0.3	0.2	44.3	--	6.0	7,572	17.57	Bowernan 1969
Peach pits	49.14	6.34	0.48	0.02	43.52		1.10	8,367	19.42	Rossi
Peach pits	53.00	5.90	0.32	0.05	39.14		1.03	8,970	20.82	Jenkins and Ebeling
Peanut hulls	45.77	5.46	1.63	0.12	39.56		5.89	8,031	18.64	Jenkins and Ebeling
Pine	51.27	6.19	0.13	0.13	42.13	0.02	0.13	8,748	20.30	Feldman et. al.
Pine bark	52.3	5.8	0.2	0.0	38.8		2.9	8,780	20.38	Tillman 1978
Pine needles	48.21	6.57			43.72		1.50	8,669	20.12	Grover and Anuradha
Pine, long leaf, bark	56.40	5.50			37.40		0.70	9,380	21.77	Risser
Pine, ponderosa	49.25	5.99	0.06	0.03	44.36		0.29	8,470	19.66	Jenkins and Ebeling
Pine, slash, bark	56.20	5.40			37.30		0.70	9,380	21.77	Risser
Pine, white	52.60	6.10			41.20		0.10	8,919	20.70	Johnson and Auth
Pine, yellow	52.60	7.00			52.60		1.31	9,668	22.44	Riser
Pine. Loblolly, bark	56.30	5.60			37.70		0.40	9,384	21.78	Risser
Pistachio shells	48.79	5.91	0.56	0.01	43.41		1.13	8,298	19.26	Jenkins and Ebeling
Poplar	48.45	5.85	0.47	0.01	43.69		1.33	8,350	19.38	Jenkins and Ebeling
Poplar	51.6	6.3	0.0	0.0	41.5		0.6	8,920	20.70	Tillman 1978
Poplar - coarse	50.82	5.89	0.59	0.02	41.08	0.04	1.60	8,139	18.89	Miles et. al. 1995
Poplar, hybrid	50.18	6.06	0.60	0.02	40.44	0.01	2.70	8,178	18.98	Miles et. al. 1995
Redwood	53.5	5.9	0.1	0.0	40.3		0.2	9,040	20.98	Tillman 1978
Redwood wastewood	53.4	6.0	0.1	0.1	39.9		0.6	9,163	21.27	Boley and Landers 1969
RDF - Tacoma, WA	39.70	5.78	0.80	0.35	27.24		26.13	6,679	15.50	Miles et. al. 1995
Rice hulls	38.30	4.36	0.83	0.06	35.45		20.60	6,415	14.89	Rossi
Rice hulls	38.5	5.7	0.5	0.0	39.8		15.5	6,610	15.34	Tillman 1978
Rice husk	38.92	5.10	2.17	0.12	37.89		15.80	6,751	15.67	Maheshwari
Rice husk bran	39.82	5.12	0.55	0.00	36.77		18.64	6,588	15.29	Channiwala
Rice straw	39.2	5.1	0.6	0.1	35.8		19.2	6,540	15.18	Tillman 1978
Rice straw	41.78	4.63	0.70	0.08	36.57		13.42	7,014	16.28	Jenkins and Ebeling
Sawdust	51.33	6.13	0.12	0.02	41.97	0.07	0.36	8,802	20.43	Feldman et. al.

Material	C	H	N	S	O	Cl	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Sawdust pellets	47.2	6.5	0.0	0.0	45.4		1.0	8,814	20.46	Wen et. al. 1974
Shredded currency	42.89	5.97	1.75	0.30	43.62		5.47	7,867	18.26	Miles et. al. 1995
Softwood	50.80	6.25	0.15	0.14	41.74	0.03	0.78	8,771	20.36	Feldman et. al.
Southern oak	49.94	5.30	0.16	0.00	42.77	0.02	0.81	8,500	19.73	Feldman et. al.
Spruce	51.80	5.70			38.30		3.80	8,759	20.33	Johnson and Auth
Sudan grass	44.58	5.35	1.21	0.01	39.18		8.65	7,492	17.39	Jenkins and Ebeling
Switchgrass, Columbus, OH	46.68	5.82	0.77	0.19	37.57	0.03	8.97	7,766	18.02	Miles et. al. 1995
Switchgrass, Dakota Leaf, MN	47.45	5.75	0.74	0.08	42.37	0.03	3.61	8,014	18.60	Miles et. al. 1995
Switchgrass, G Petersen 1	48.64	5.46	0.04	0.07	42.06	0.005	3.73	8,001	18.57	Iowa Project
Switchgrass, G Petersen 2	47.98	5.46	0.19	0.06	41.54	0.007	4.77	7,765	18.02	Iowa Project
Switchgrass, G Petersen 4	48.37	5.52	0.03	0.15	43.59	0.003	2.34	8,104	18.81	Iowa Project
Switchgrass, Joe Cross 1	47.11	5.39	0.23	0.06	43.19	0.007	4.02	7,934	18.41	Iowa Project
Switchgrass, Joe Cross 2	46.00	4.57	0.32	0.05	44.51	0.006	4.54	7,862	18.25	Iowa Project
Switchgrass, Joe Cross 4	48.00	5.54	0.16	0.07	42.61	0.004	3.61	8,017	18.61	Iowa Project
Switchgrass, Krutsinger 1	46.91	5.38	0.38	0.07	41.61	0.017	5.64	7,890	18.31	Iowa Project
Switchgrass, Krutsinger 2	44.97	5.10	0.69	0.09	42.43	0.024	6.72	7,812	18.13	Iowa Project
Switchgrass, Krutsinger 4	48.20	5.68	0.24	0.06	42.00	0.017	3.81	7,952	18.46	Iowa Project
Switchgrass, Lodge Land 1	47.71	5.43	0.38	0.04	41.53	0.007	4.91	7,953	18.46	Iowa Project
Switchgrass, Lodge Land 2	47.46	5.41	0.48	0.05	43.18	0.007	3.42	8,091	18.78	Iowa Project
Switchgrass, Lodge Land 4	47.72	5.48	0.15	0.06	43.10	0.003	3.49	8,034	18.65	Iowa Project
Switchgrass, Schulz 30	48.69	5.61	0.06	0.05	43.14	0.003	2.44	8,012	18.60	Iowa Project
Switchgrass, Sellers 1	48.69	5.50	0.34	0.06	41.28	0.004	4.14	8,021	18.62	Iowa Project
Switchgrass, Sellers 2	48.31	5.52	0.29	0.09	42.59	0.005	3.20	8,074	18.74	Iowa Project
Switchgrass, Sellers 32	49.10	5.71	0.17	0.05	42.21	0.002	2.76	7,983	18.53	Iowa Project
Switchgrass, Sellers 4	48.72	5.54	0.16	0.05	41.70	0.008	3.83	8,052	18.69	Iowa Project
Switchgrass, Summer, MN	47.51	5.02	0.65	0.07	37.02	0.03	2.69	7,979	18.52	Miles et. al. 1995
Switchgrass, SWG10	43.78	5.25	0.52	0.07	46.10	0.035	4.29	7,806	18.12	Iowa Project
Switchgrass, SWG12	43.20	5.23	0.50	0.10	47.19	0.046	3.78	7,735	17.95	Iowa Project
Switchgrass, SWG14	42.13	5.07	0.54	0.08	48.49	0.022	3.68	7,803	18.11	Iowa Project
Switchgrass, SWG16	42.89	5.05	0.57	0.10	47.68	0.015	3.71	7,837	18.19	Iowa Project
Switchgrass, SWG18	43.93	5.17	0.55	0.08	46.86	0.005	3.41	7,809	18.12	Iowa Project
Switchgrass, SWG20	44.21	5.07	0.64	0.09	46.23	0.004	3.75	7,793	18.09	Iowa Project

Material	C	H	N	S	O	Cl	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Switchgrass, SWG22	44.45	5.14	0.59	0.11	46.17	0.004	3.53	7,847	18.21	Iowa Project
Switchgrass, SWG26	44.86	5.15	0.57	0.09	46.20	0.005	3.13	7,852	18.22	Iowa Project
Switchgrass, SWG28	44.71	5.15	0.63	0.07	45.90	0.003	3.55	7,785	18.07	Iowa Project
Switchgrass, Van Patten 1	48.32	5.50	0.10	0.06	42.80	0.036	3.21	8,161	18.94	Iowa Project
Switchgrass, Van Patten 2	48.41	5.48	0.09	0.04	42.56	0.024	3.42	8,091	18.78	Iowa Project
Switchgrass, Van Patten 4	46.95	5.79	0.14	0.06	44.71	0.012	2.35	8,182	18.99	Iowa Project
Switchgrass, WG24	44.03	5.09	0.55	0.09	46.30	0.006	3.93	7,864	18.25	Iowa Project
Urban wood waste	48.77	5.76	0.27	0.07	39.59	0.05	2.50	8,361	19.41	Miles et. al. 1995
Walnut shells	49.98	5.35	0.21	0.01	43.35		0.56	8,695	20.18	Jenkins and Ebeling
Walnut, English, prunings	49.72	5.63	0.37	0.01	43.14		1.08	8,458	19.63	Jenkins and Ebeling
Water hyacinth	40.30	4.60	1.51		33.99		19.60	6,402	14.86	Klass and Ghosh
Water hyacinth	43.00	5.80	5.60		29.50		15.30	7,747	17.98	Elliot et al
Wheat dust	41.38	5.10	3.04	0.19	35.17		13.68	6,980	16.20	Jenkins and Ebeling
Wheat straw	43.20	5.00	0.61	0.11	39.40		8.90	7,199	16.71	Jenkins and Ebeling
Willow - SA22 -3 yr	49.90	5.90	0.61	0.07	41.81	<0.01	1.71	8,424	19.55	Miles et. al. 1995
Willow - SA22 Butt	48.95	6.05	0.36	0.04	43.54	0.01	1.06	8,326	19.32	Miles et. al. 1995
Willow - SA22 Top	49.42	5.89	0.96	0.12	41.27	<0.01	2.34	8,510	19.75	Miles et. al. 1995
Willow - SA22-1 yr	49.75	6.00	0.65	0.09	42.01	0.01	1.50	8,457	19.63	Miles et. al. 1995
Willow - SH3-1 yr	48.85	6.04	0.71	0.06	42.64	0.01	1.70	8,443	19.60	Miles et. al. 1995
Willow - SP3-1yr	50.29	6.01	0.50	0.07	41.93	<0.01	1.20	8,691	20.17	Miles et. al. 1995
Willow - SV1-1 yr	47.94	5.84	0.63	0.06	44.43	<0.01	1.10	8,325	19.32	Miles et. al. 1995
Willow - SV1-3 yr	49.09	5.89	0.35	0.03	46.39	<0.01	0.95	8,330	19.33	Miles et. al. 1995
Wood - land clearing	42.32	5.02	0.33	0.06	35.77	0.02	16.50	7,408	17.19	Miles et. al. 1995
Wood - yard waste	41.54	4.79	0.85	0.24	32.21	0.30	20.37	7,009	16.27	Miles et. al. 1995

Figure 3-1: Nitrogen Content of Selected Biomass Samples

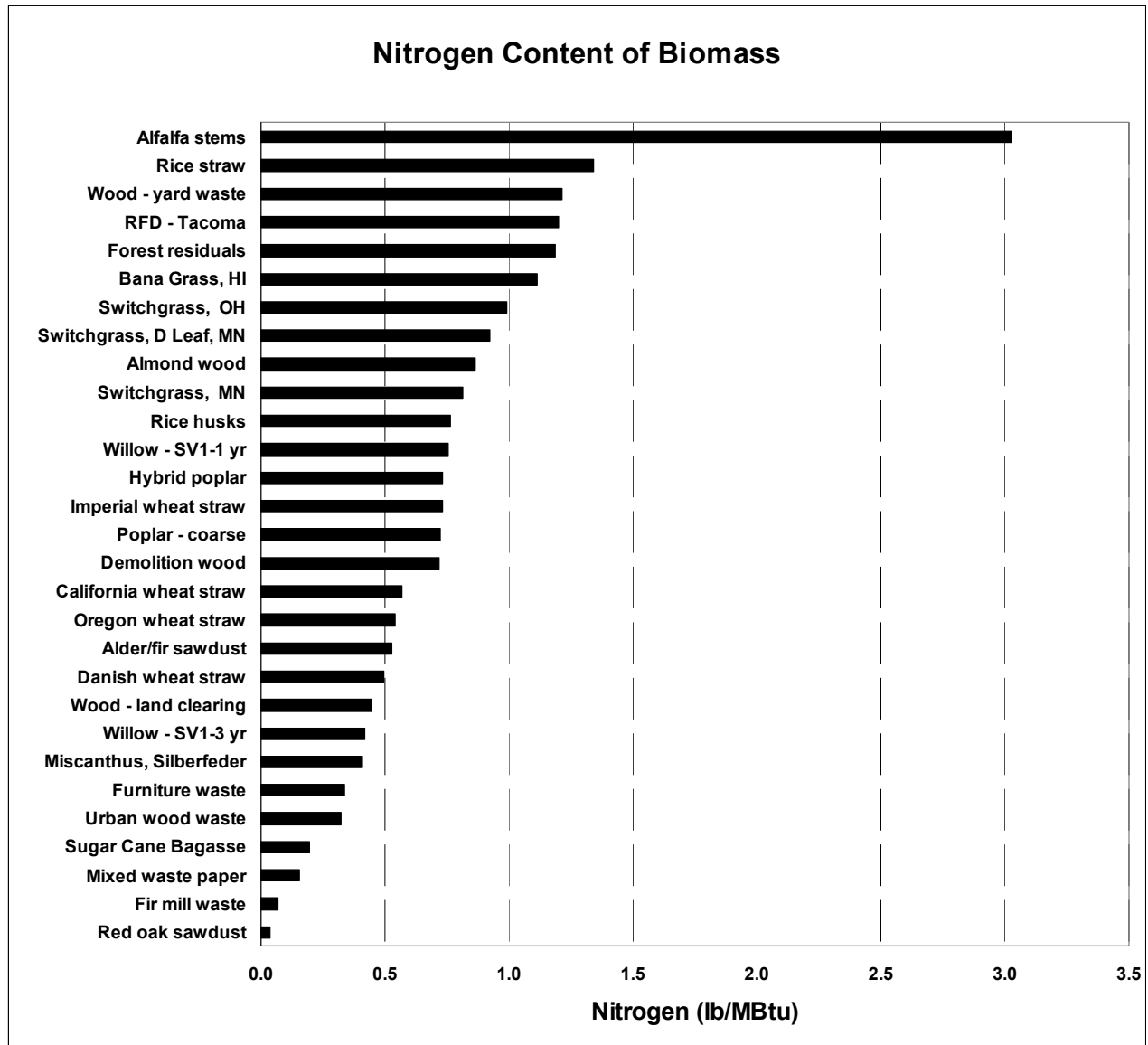


Figure 3-2: Potassium Content of Selected Biomass Samples³

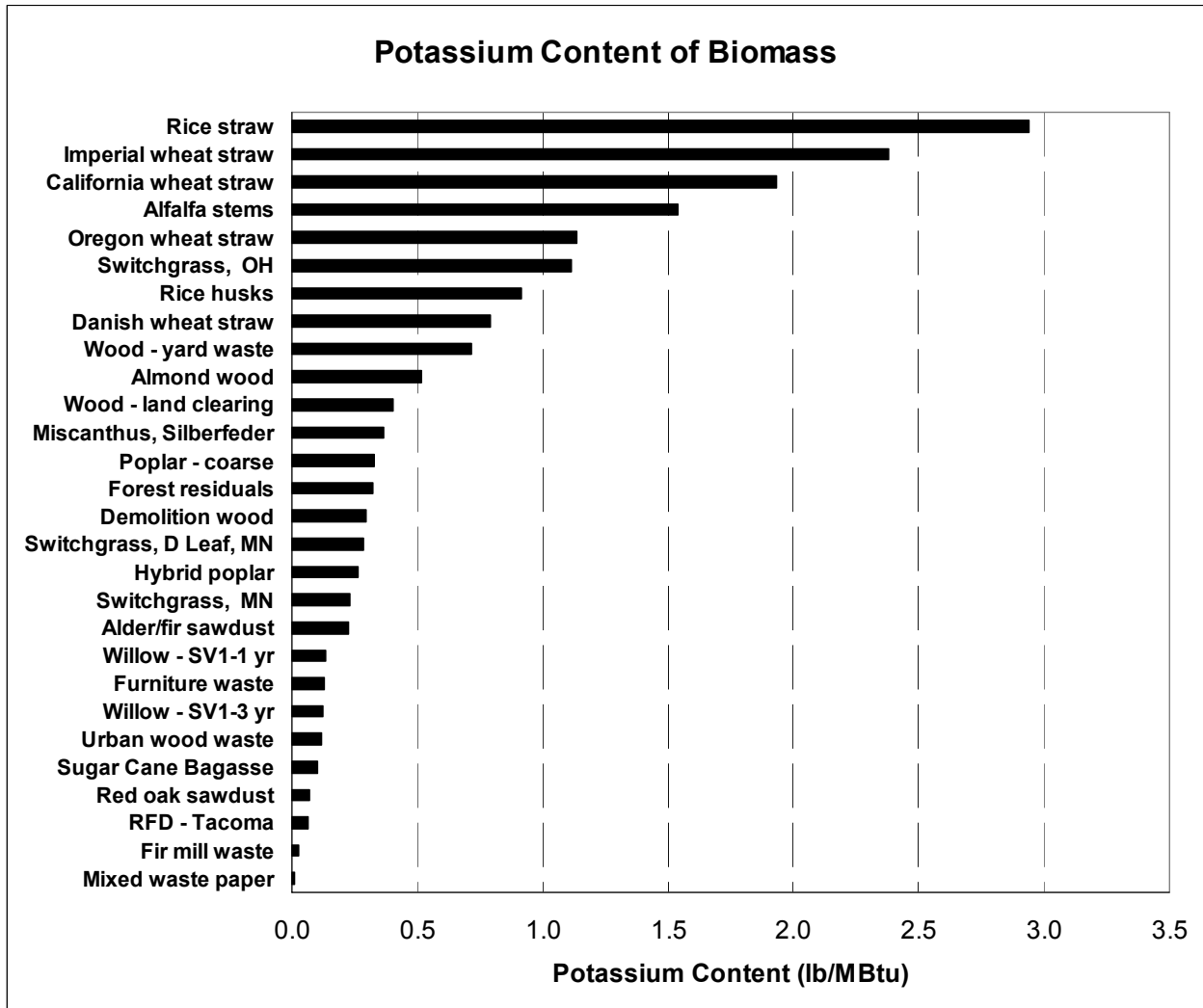


Table 3-5: Elemental Analysis of Volatiles Liberated by Pyrolysis for Two Selected Fuels

Fuel	wt% in volatile, dry basis			Molar ratio volatile		
	C	H	O	C	H	O
Lignite	17.4	4.22	19.17	1	2.91	0.83
Douglas fir bark	23.4	5.9	36.7	1	3.03	1.17

The C/H/O ratios of these volatile fractions are very similar despite the difference in feedstock. In the pyrolysis process, at relatively high temperatures,



If we assume that CO is produced exclusively we can calculate the product analysis from pyrolysis.

Therefore, assuming:



let X be the moles of carbon converted to methane, Y the oxygen converted to water, and Z the carbon to CO.

The material balance equations yield:

$$X = [2 + (\text{H}/\text{C}) - 2 (\text{O}/\text{C})] / 6 \quad (3-9)$$

$$Z = 1 - X \quad (3-10)$$

$$Y = \text{O}/\text{C} - Z \quad (3-11)$$

In the calculation for methane it should be pointed out that as long as water-gas shift reaction equilibrium is attained, it makes no difference whether the non-hydrocarbon products are CO and H₂O or a mixture of CO, CO₂, H₂, and H₂O.

Table 3-6 presents such an analysis on a dry basis of 100 lb of fuel.

Table 3-6: Evaluation of Feedstocks for Pyrolysis by Material Balance Calculation

Fuel	SCF Gas	Mole Fractions			Lb C in CH ₄
	100lb dry feed	CH ₄	CO	H ₂ O	100lb C in feed
Lignite	754	0.395	0.334	0.271	14.7
Douglas fir bark	1196	0.277	0.341	0.382	18.7

The gas derived from lignite is higher in quality than that from the fir bark due to the bark's greater potential to form water. The quantity of gas produced is greater for the fir bark due to the greater quantity of volatiles present. The most important factor is the fraction of carbon converted to methane. The woody material shows a greater potential to form methane on a carbon feed basis, indicating that it is a higher quality feedstock for pyrolysis. This may be attributed to the higher degree of aromaticity exhibited in coals.

Table 3-7 presents ultimate analysis for typical pyrolysis chars derived from biomass feedstocks. Except for the municipal solid waste char, all contain considerable quantities of volatile constituents, including H and O, due to the low processing temperature.

The C/H and C/O ratios are greater in all chars than in the fresh feed materials. The high-temperature municipal waste char has been almost completely devolatilized, as is evidenced by the low H and O contents.

3.1.3 Moisture Content of Fuels

Woody fuels and municipal solid waste samples are available with various moisture contents. The moisture is important in determining drying costs and as-received heat contents of the fuels.

Table 3-8 presents approximate ranges of moisture for typical biomass fuels. The effect of moisture on the recoverable heat is dramatic due to the heat requirements for vaporizing the moisture plus superheating the vapor.

Table 3-7: Ultimate Analysis Data for Selected Pyrolysis Chars
(Dry Basis, Weight Percent)

Material	C	H	N	S	O	Ash	HHV Btu/lb	HHV MJ/kg	Reference
Fir bark char	49.9	4.0	0.1	0.1	24.5	21.4	8,260	19.17	Pober and Bauer 1977
Rice hull char	36.0	2.6	0.4	0.1	11.7	49.2	6,100	14.16	Pober and Bauer 1977
Grass straw char	51.0	3.7	0.5	0.8	19.7	24.3	8,300	19.26	Pober and Bauer 1977
Animal waste char ^a	34.5	2.2	1.9	0.9	7.9	48.8	5,450	12.65	Pober and Bauer 1977
MSW char	54.9	0.8	1.1	0.2	1.8	41.2	8,020	18.61	Sanner et al 1970
Redwood charcoal (421 - 549°C)	75.6	3.3	0.2	0.2	18.4	2.3	12,400	28.78	Boley and Landers 1969
Redwood charcoal (460 - 941°C)	78.8	3.5	0.2	0.2	13.2	4.1	13,100	30.41	Boley and Landers 1969
Oak charcoal (438 - 641°C)	67.7	2.4	0.4	0.2	14.4	14.9	10,660	24.60	Boley and Landers 1969
Oak charcoal (571°C)	64.6	2.1	0.4	0.1	15.5	17.3	9,910	23.00	Boley and Landers 1969

^aContains 3.7% Cl lumped with oxygen

Table 3-8: Approximate Moisture Contents Of Typical Biomass Fuels

Biomass Fuel	Moisture Content (wt %)
Bark	25 - 75
Coarse wood residue	30 - 60
Manure, beef cattle	80 - 90
Manure, poultry	70 - 80
Shavings	16 - 40
Sawdust	25 - 40
Sander dust	2 - 8
Municipal refuse	20
Air dry feedlot waste	12
Baled switchgrass	10 - 15

3.1.4 Heating Values

The heating value of carbon feedstocks is determined by the ASTM method listed in Table 3-1. The experimental method employs an adiabatic bomb calorimeter which measures the enthalpy change between reactants and products at 25°C. The heating value obtained is termed the higher heating value because the water of combustion is present in the liquid state at the completion of the experimental determination.

The heating value may be reported on two bases. These are the gross or higher heating value and the net or lower heating value. The higher heating value (HHV) represents the heat of combustion relative to liquid water as the product. The lower heating value (LHV) is based on gaseous water. You may also see HHV and LHV referred to as gross calorific value (GCV) and net calorific value (NCV). The difference in the heating value is the latent heat of the water of combustion. Heating values often are reported on both wet and dry fuel bases. The conversion between bases is simple in the case of the higher heating value, involving only normalizing out the moisture (M). This is true because the moisture present in the raw fuel is in the same state before and after combustion.

$$\text{HHV}^* = \text{HHV} / (1 - M) \quad (3-12)$$

Lower (net) heating values depend on the moisture content in a more complicated

fashion. Since both the product water and moisture are present as vapor after combustion, a portion of the heat of combustion is used to evaporate the moisture. Therefore, using the latent heat of water, $\lambda = 980$ Btu/lb,

$$\text{HHV}^* = (\text{LHV} - M\lambda) / (1 - M) \quad (3-13)$$

To convert between higher (gross) and lower (net) heating values, the amount of water produced by combustion reactions, but not including moisture, must be known. If this is called W , lb water/lb fuel, then the heating values are related by:

$$\text{HHV} = \text{LLV} + W\lambda. \quad (3-14)$$

All heats reported in this discussion are higher (gross) heating values on a dry basis.

Table 3-4 reports higher heating values on a dry basis for a variety of biomass fuels. Typically, the heating values for coals are much greater than for biomass materials, ranging from 10 MBtu/lb to 14 MBtu/lb (23.2 MJ/kg to 32.5 MJ/kg) and 5 MBtu/lb to 9 MBtu/lb (11.6 MJ/kg to 20.9 MJ/kg), respectively. This is principally due to the higher carbon content of the coals. Table 3-7 gives higher heating values for biomass chars. The values are low due to the high ash content of the chars; however, on a dry, ash-free basis, the heating values are similar to those of the coals.

A common method for estimating heating values of solid fuels is the Boie equation (Van Krevelan 1961) which permits the heating value to be estimated from the ultimate analysis. The Boie equation has been used to estimate the HHV of the biomass samples in Table 3-4. The average absolute error of the estimate is 4.70%, with a bias of 3.19%. A second method for estimating heating values is that of Tillman (1978). As shown in Table 3-9, the results for Tillman's equation, which uses only the carbon content, give comparable values. The average error is roughly 2.83% with a positive bias of 0.83%.

A third method of estimating gross heating values has been developed at IGT (Institute of Gas Technology 1978) using the experimental heating values and ultimate analyses of more than 700 coal samples. When this heating value correlation is used to estimate the higher heating values of fresh biomass materials, the average error is 3.34% with a negative 1.73% bias.

A linear least-squares regression has been performed on the biomass data set in Table 3-4 and the resulting regression equation is given in Table 3-9. The average error is 2.02%, with a positive bias of 0.09. R^2 for the fit is 0.900. A graphical representation of the correlation versus data is given in Figure 3.3. While this better represents the data in Table 3-4, it must be noted that the estimate has not been checked for biomass samples outside the given data set. The experimental error in the ASTM heating value is ± 100 Btu/lb while the regression yields an average error for chars and fresh biomass

of about ± 160 Btu/lb. Experimental values should be used in cases where the elemental analysis is much different from materials previously tested.

Table 3-9: Comparison of Experimental and Calculated Higher (Gross) Heating Values

Name	Equation HHV [=] Btu/lb	Absolute Avg Error %	Bias %	R ²
Boie (1)	157.4 C + 520.4 H + 28.1 N + 46.9 S - 49.7 O	4.70	3.19	--
Tillman (2)	188 C - 718	2.83	0.83	--
IGT (3)	146.58 C + 568.78 H + 29.45 S - 6.58 A - 51.53 (O + N)	3.34	-1.73	--
Bain (4)	85.65 + 137.04 C + 217.55 H + 62.56 N + 107.73 S + 8.04 O - 12.94 A (Eq 3-15)	2.02	0.09	0.900

- (1) Van Krevelan, D.W. (1961). Coal; Coal Science and Technology 3, Elsevier Scientific Publishing Company, NY, NY, page 416
- (2) Tillman, D.A. (1978). Wood as an Energy Source, Academic Press, NY, NY.
- (3) Institute of Gas Technology (1978). "Coal Conversion Systems Technical Data Book," DOE Contract EX-76-C-01-2286, available from NTIS.
- (4) This publication

To convert to MJ/kg multiply by 0.00232

Nomenclature: All values are in weight percent, dry basis

A = ash
C = carbon
H = hydrogen
N = nitrogen
O = oxygen
S = sulfur

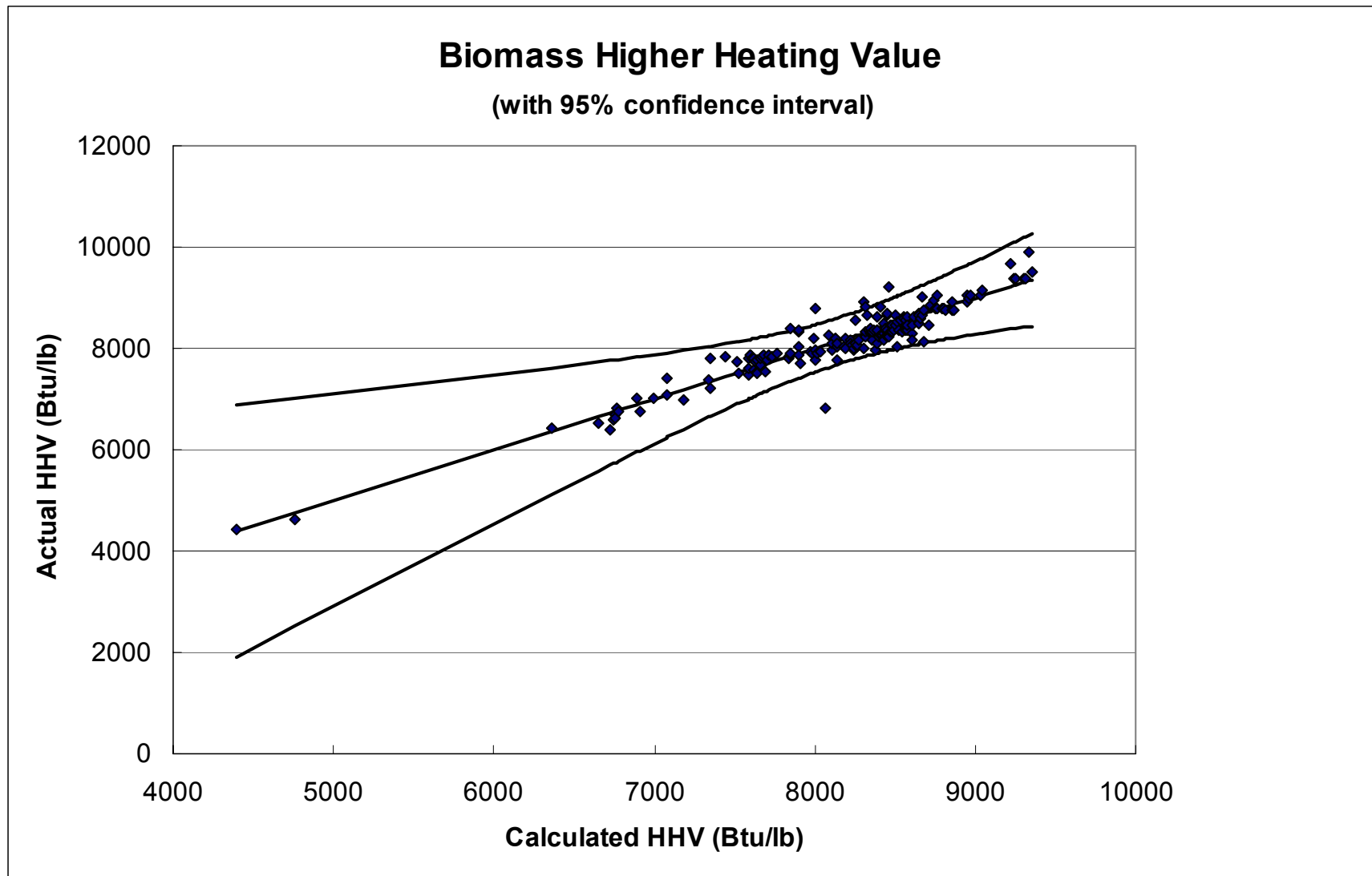
% Error = $100 (\text{calc. HHV} - \text{Exptl. HHV}) / \text{Exptl. HHV}$

Absolute Average Error = $\sum (\text{absoute error})_i / n$

Bias = $\sum (\text{Error})_i / n$

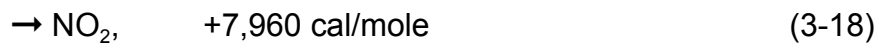
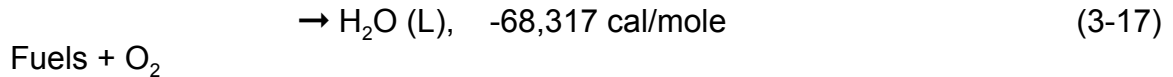
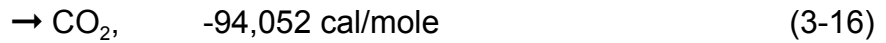
where n =175

Figure 3-3: Biomass Higher Heating Value



3.1.5 Heats of Formation

In thermodynamic calculations, the heat of formation of the feedstocks is required. Heats of formation may be calculated rigorously from the heats of combustion, assuming that the only materials oxidized are C, H, N, and S, by posing the following reactions:



The heat of formation of the fuel may be calculated as follows, assuming no chemical heat involving ash reactions:

$$H_f (25^\circ\text{C}) = (\text{HHV}^* + 0.018 \sum_{\text{Prod}} [H_{fi} n_{fi}]) / (1 - \text{Ash}) \quad (3-20)$$

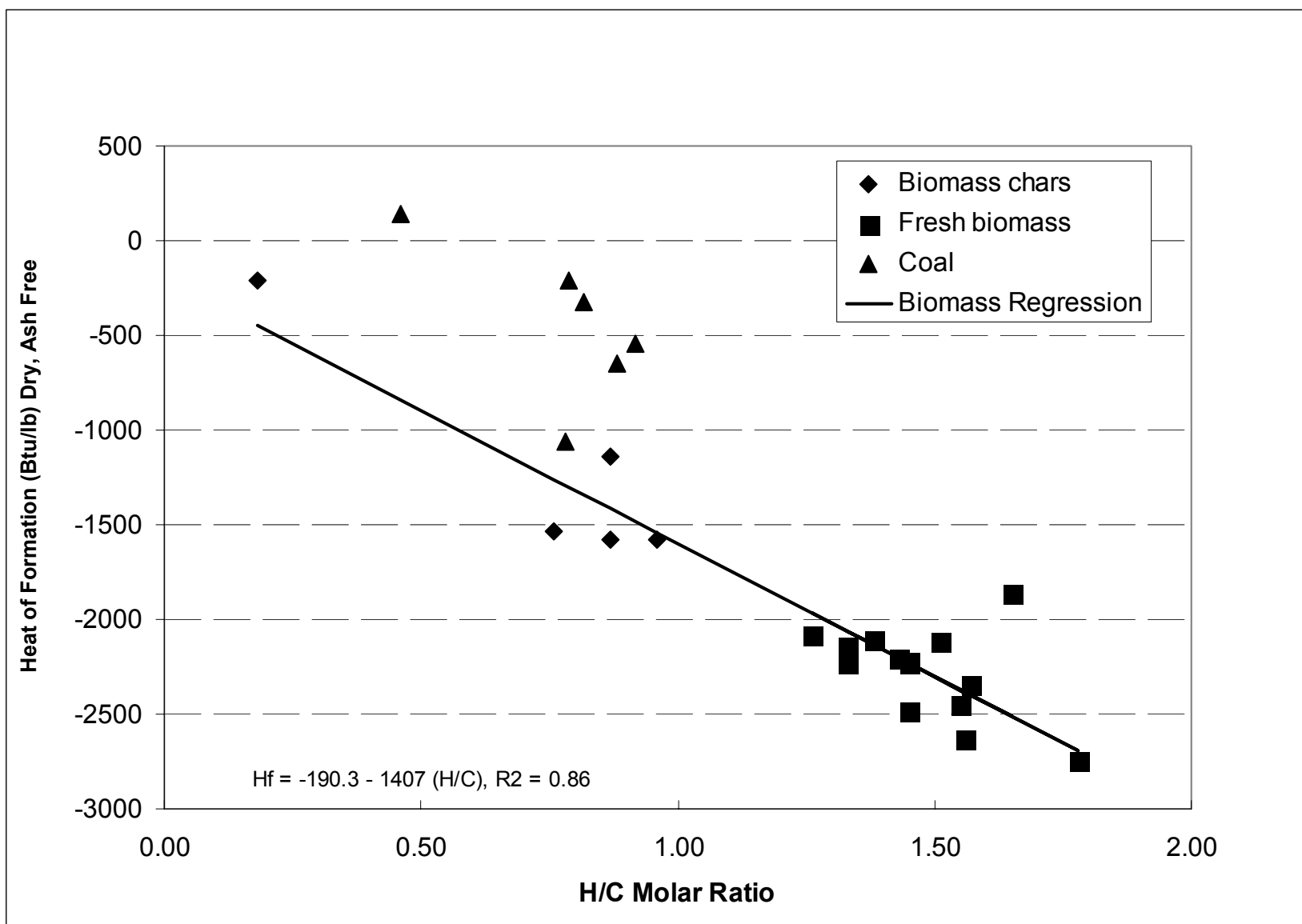
in Btu/lb, dry, ash-free basis.

In this equation, n_{fi} is the moles of species i formed per 100 lb of dry biomass on combustion (i can be CO_2 , $\text{H}_2\text{O(L)}$, NO_2 , SO_2) while H_{fi} is the heat of formation of i at 25°C in cal/mole. The factor 0.018 puts the formation enthalpy on a Btu per pound of biomass basis. The HHV is treated as a positive number. The heat of formation is normalized to a dry, ash-free basis for purposes of comparison. Table 3-10 presents heat of formation for a variety of feedstocks. The data show a definite trend in terms of the rank (degree) of aromatization of the materials involved. Biomass is very low in rank since its structure consists of only single aromatic rings (benzene derivatives). Fuels of higher rank - peat, lignite, bituminous, and anthracite coals - have structures containing progressively larger aromatic clusters. Typical bituminous coal structures contain from four to six condensed aromatic rings. The fuel of highest rank is graphite. The coals tend to have low heats of formation which increase in the exothermic sense as the rank decreases. Most woody materials exhibit a constant heat of formation in the range of -2,200 Btu/lb. Materials such as straw and rice hulls have higher heats of formation, on the order of -2,700 Btu/lb. The biomass chars generally exhibit heats of formation intermediate between coals and fresh biomass materials. Figure 3-4 shows how the heats of formation depend on the H/C ratio of the feedstock. It is evident that the biomass chars, although similar in ultimate analysis to coals do not correlate with the coals in terms of H/C ratio. This is probably due to the coal's greater degree of aromatization, which is a result of the coalification process.

**Table 3-10: Heats of Formation for Typical
Fuels and Biomass Materials**
(Basis: Dry, Ash-Free Solid)

Material	Hf (77°F) (Btu/lb)	H'/C'
Charcoal	142	0.46
Pittsburgh seam coal	-209	0.79
Western Kentucky No. 11 coal	-323	0.82
Utah coal	-540	0.92
Wyoming Elkol	-648	0.88
Lignite	-1062	0.78
Douglas fir	-2219	1.45
Douglas fir bark	-2081	1.26
Pine bark	-2227	1.33
Western hemlock	-2106	1.38
Redwood	-2139	1.33
Beech	-2480	1.45
Hickory	-2344	1.57
Maple	-2203	1.43
Poplar	-2229	1.45
Rice hulls	-2747	1.78
Rice straw	-2628	1.56
Sawdust pellets	-1860	1.65
Animal waste	-2449	1.55
Municipal solid waste	-2112	1.51
Fir bark char	-1580	0.96
Municipal solid waste char	-1136	0.87
Grass straw char	-1581	0.87
Animal waste char	-1536	0.76
Municipal solid waste char	-214	0.18

Figure 3-4: Heats of Formation of Carbonaceous Fuels



Heats of combustion for biomass materials can be calculated using the heat of formation data based on the following empirical correlation for biomass materials:

$$H_f (77^\circ \text{ F}) = - 190.3 - 1407 \text{ H}'/\text{C}' \quad (3-21)$$

with H'/C' as mole ratio, Btu/lb, dry ash-free basis.

For natural biomass materials and their chars, the following equation results, based on the ultimate analysis and the pertinent combustion reactions:

$$\text{HHV}^* = (141\text{C} + 615\text{H} - 10.2\text{N} + 39.8\text{S}) - (1 - \text{A}/100)[(16,769\text{H}/\text{C}) + 190] \quad (3-22)$$

The HHV^* is the gross heating value on a dry basis, Btu/lb, and the analytical data are expressed in weight percent. This equation cannot be expected to function for manmade materials such as plastics or for non-cellulose-derived materials like leather. For the biomass data set in Table 3-4, the average absolute error is 2.52% and the bias is -0.47%.

3.1.6 Ash

The ash content of selected biomass samples is given in Table 3-11. Biomass with high annual growth, such as herbaceous materials, annual crops, and woody prunings all have abundant alkali in the ash. Potassium is of primary importance because it volatilizes and reacts during combustion. In addition, biomass rich in both potassium and chlorine can cause large amounts of slagging and fouling during combustion. Biomass ash samples are typically low in sodium content because sodium is toxic to non-halophytic plants. Ash samples high in iron typically indicate presence of non-biomass materials such as dirt or soil.

Table 3-11: Ash Composition of Selected Biomass Samples

Material		Ash wt%	Elemental Composition, wt%												
			SiO2	Al2O3	TiO2	Fe2O3	CaO	MgO	Na2O	K2O	SO3	P2O5	CO2/Other	Undet.	
Mixed waste paper		8.33	28.10	52.56	4.29	0.81	7.49	2.36	0.53	0.16	1.70	0.20		1.80	
Fir mill waste		0.41	15.17	3.96	0.27	6.58	11.90	4.59	23.50	7.00	2.93	2.87	18.92	2.31	
RFD - Tacoma		26.13	33.81	12.71	1.66	5.47	23.44	5.64	1.19	0.20	2.63	0.67		12.58	
Red oak sawdust		0.31	20.97	2.99	0.27	2.94	10.90	4.15	1.40	22.40	2.69	1.33	14.30	15.66	
Sugar Cane Bagasse		2.44	46.61	17.69	2.63	14.14	4.47	3.33	0.79	4.15	2.08	2.72		1.39	
Urban wood waste		5.54	55.12	12.49	0.72	4.51	13.53	2.93	3.19	4.78	1.92	0.88		-0.07	
Willow - SV1-3 yr		0.95	8.08	1.39	0.06	0.84	45.62	1.16	2.47	13.20	1.15	10.04	13.67	2.32	
Furniture waste		3.61	57.62	12.23	0.50	5.63	13.89	3.28	2.36	3.77	1.00	0.50		-0.78	
Willow - SV1-1 yr		1.10	16.76	3.01	0.07	0.85	34.83	2.46	3.05	12.20	1.70	10.36	17.58	-2.87	
Alder/fir sawdust		4.13	35.36	11.54	0.92	7.62	24.90	3.81	1.71	5.75	0.78	1.90	1.85	3.86	
Switchgrass, MN		2.69	61.64	1.32	0.19	1.08	11.11	4.86	0.64	8.24	0.80	3.09		7.03	
Hybrid poplar		2.70	5.90	0.84	0.30	1.40	49.92	18.40	0.13	9.64	2.04	1.34	8.18	1.91	
Switchgrass, D Leaf, MN		3.61	61.23	0.57	0.37	0.79	12.06	5.42	0.43	7.63	1.11	3.56		6.83	
Demolition wood		13.12	45.91	15.55	2.09	12.02	13.51	2.55	1.13	2.14	2.45	0.94		1.71	
Forest residuals		3.97	17.78	3.55	0.50	1.58	45.46	7.48	2.13	8.52	2.78	7.44		2.78	
Poplar - coarse		1.60	0.88	0.31	0.16	0.57	44.40	4.32	0.23	20.08	3.95	0.15	19.52	5.43	
Miscanthus, Silberfeder		3.05	61.84	0.98	0.05	1.35	9.61	2.46	0.33	11.60	2.63	4.20		4.95	
Wood - land clearing		16.50	65.77	14.84	0.55	5.27	5.78	1.81	2.70	2.19	0.36	0.66	0.45	-0.38	
Almond wood		6.78	45.60	10.75	0.54	4.06	18.96	4.22	3.08	6.26	2.06	1.47		3.00	
Wood - yard waste		20.37	59.65	3.06	0.32	1.97	23.75	2.15	1.00	2.96	2.44	1.97		0.73	
Danish wheat straw		3.89	55.32	0.84	0.22	1.05	12.27	2.48	1.51	12.90	2.49	4.30		6.62	
Rice husks		20.26	91.42	0.78	0.02	0.14	3.21	0.01	0.21	3.71	0.72	0.43			
Switchgrass, OH		8.97	65.18	4.51	0.24	2.03	5.60	3.00	0.58	11.60	0.44	4.50		2.32	
Oregon wheat straw		4.32	46.07	1.69	0.09	1.85	9.95	2.45	1.18	25.20	4.92	3.32		3.28	
Alfalfa stems		5.27	5.79	0.07	0.02	0.30	18.32	10.38	1.10	28.10	1.93	7.64	14.80	11.55	
California wheat straw		7.02	55.32	1.88	0.08	0.73	6.14	1.06	1.71	25.60	4.40	1.26		1.82	
Imperial wheat straw		9.55	37.06	2.23	0.17	0.84	4.91	2.55	9.74	21.70	4.44	2.04		14.32	
Rice straw		18.67	74.67	1.04	0.09	0.85	3.01	1.75	0.96	12.30	1.24	1.41		2.68	
Bana Grass, HI		9.88	33.65	0.80	0.07	0.63	3.57	1.71	0.38	42.80	0.85	2.74	8.97	3.83	

3.2 CHEMICAL COMPOSITION OF WOODS

In characterizing and correlating reactivity data for pyrolysis and gasification, it is necessary to have some idea of the chemical structure of the reactant material. Woods can be analyzed in terms of fractions of differing reactivity by solvent extraction techniques. This discussion provides some of the relevant information on the structure and composition of these reactive fractions which will be useful in discussions of gasification kinetics and pyrolysis.

Woods can be separated into three fractions: extractables, cell wall components, and ash. The extractables, generally present in amounts of 4% to 20%, consist of materials derived from the living cell. The cell wall components, representing the bulk of wood, are principally the lignin fraction and the total carbohydrate fraction (cellulose and hemicellulose) termed holocellulose. Lignin, the cementing agent for the cellulose fibers, is a complex polymer of phenylpropane. Cellulose is a polymer formed from d (+)-glucose while the hemicellulose polymer is based on other hexose and pentose sugars. In woods, the cell wall fraction generally consists of lignin/cellulose in the ratio 43/57. Residues of the total wood, such as bark and sawdust, have differing compositions.

Table 3-12 presents some analyses of woods on a dry basis while Table 3-13 presents data for typical wood barks.

Table 3-12: Chemical Analyses of Representative Woods ^a
(wt % Dry Basis)

Sample	Ash	Extractables	Lignin	Holocellulose
Softwoods ^b				
Western white pine	0.20	13.65	26.44	59.71
Western yellow pine	0.46	15.48	26.65	57.41
Yellow cedar	0.43	14.39	31.32	53.86
Incense cedar	0.34	20.37	37.68	41.60
Redwood	0.21	17.13	34.21	48.45
Hardwoods ^c				
Tanbark oak	0.83	16.29	24.85	58.03
Mesquite	0.54	23.51	30.47	45.48
Hickory	0.69	19.65	23.44	56.22

^aEncyclopedia of Chem. Tech. (1963), p. 358

^bSoftwood refers to conifer woods

^cHardwood refers to deciduous woods

Table 3-13: Chemical Analyses of Representative Wood Barks^a
(% Dry Basis)

Sample	Ash	Extractables	Lignin	Holocellulose ^b
Black spruce	2.1	24.78	45.84	24.78
Fir	3.1	30.37	39.16	27.37
White birch	1.5	21.6	37.8	39.1
Yellow birch	2.9	19.9	36.5	40.7
Beech	8.3	18.3	37.0	36.4

^aFrom Wise 1946

^bBy difference

In comparing the ultimate analysis data for barks and whole woods in Table 3-4, there is no indication that the chemical makeup of the feedstocks is different. However, from the extractable and cell wall analyses it is evident that the lignin and extractable contents of barks are much greater than those of whole woods. It should be expected that these materials would exhibit different overall reactivities due to their chemical differences.

3.2.1 Cellulose

The carbohydrate fraction of plant tissues is composed of cellulose and hemicelluloses, which are moderate to high molecular weight polymers based on simple sugars. Cellulose itself is derived from d-glucose while the hemicelluloses are principally polymers of d-xylose and d-mannose. The hemicellulose composed of pectin generally is present in only very small quantities in woody material but can be a substantially abundant constituent of the inner bark of trees. The cellulose polymer is shown in Fig. 3-5.

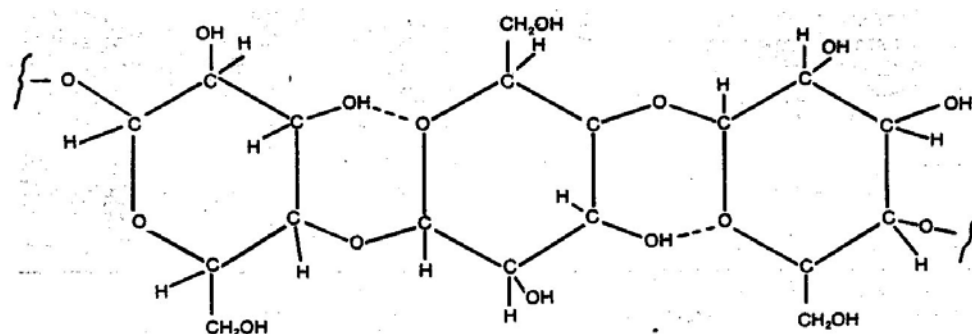


Figure 3-5: The Cellulose Molecule

Cellulose is composed of d-glucose units ($C_6H_{10}O_5$) bound together by ether-type linkages called glycosidic bonds. Glucose is a hexose, or six carbon sugar. In wood the polymers form thread-like chains of molecular weight greater than 100,000. In cotton, 3000 or more units with a combined molecular weight of 500,000 may be present in chains, yielding an extended length of 15,700 Å and cross section of 4 by 8 Å. These very long, thin molecules can be coiled and twisted but, because of the arrangement of the ether linkage, the chain is stiff and extended. An additional contribution to rigidity results from the hydrogen bonding between a hydroxyl hydrogen and the ring oxygen in the adjacent monomer. The threads are woven amongst each other in a random fashion, termed amorphous cellulose, and also fitted together in a crystalline arrangement. Strong van der Waals forces and hydrogen bonds between threads (termed secondary bonding) give rise to a lamellae structure. The weakest bond in the chain direction is the C-O glycosidic bond with an energy of 50 kcal. Cellulose fibers are thus very strong.

The dominant physical characteristic of cellulose is its extreme insolubility, which retards not only acid and enzymic hydrolysis but also the removal of lignins and hemicelluloses interspersed through the cellulose structures. The strong secondary bonding is responsible for the insolubility. Cellulose can be dissolved by strong acids such as hydrochloric, sulfuric, and phosphoric.

Pyrolysis of cell wall materials provides a mixture of volatile materials, tars, and char. The proportion of each fraction and its composition depends on the reaction conditions including temperature, pressure, heating rate, and atmospheric composition. Char results from the condensation of aromatic compounds formed from the primary decomposition products. Since aromatics are not present initially, the amount of char formed by condensation reactions is relatively small.

3.2.2 Principal Hemicelluloses

Interlaced with cellulose in the cell walls are a number of other polymeric sugars termed hemicelluloses. These are generally differentiated from true cellulose by their solubility in weak alkaline solutions. Figure 3-6 shows a sequence employed by Timell (1967) for isolating softwood polysaccharides. Hemicelluloses are not precursors of cellulose; they are distinctly different compounds that contain acidic and neutral molecules of low and high molecular weight. In contrast to cellulose, which appears to be universal and invariant as the structural polysaccharide of higher land plants, the hemicellulose polysaccharides show a significant variation in composition and structure among species. Several reviews of hemicellulose chemistry have been presented by Polglase (1955), Aspinall (1959), and Whistler and Richards (1970).

Most hemicelluloses contain two to four (and occasionally five to six) simpler sugar residues, d-xylose, d-glucose, d-mannose, d-galactose, 1-arabinose, d-glucuronic acid, and 4-O-methyl-d-glucuronic acid residues constitute the majority of hemicellulose monomers as shown in Fig. 3-7. The structure is similar to that of cellulose except that

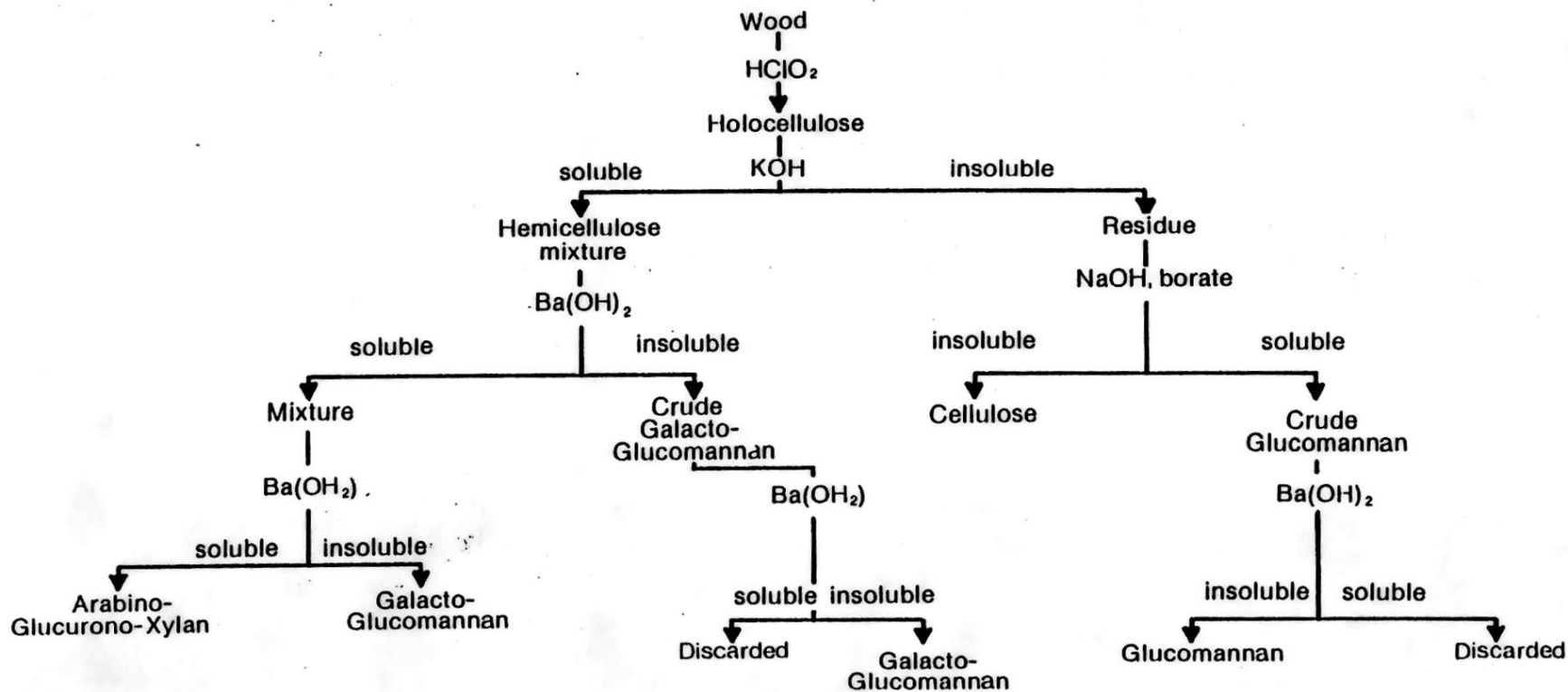


Figure 3-6: Extraction Sequence for Isolation of Softwood Polysaccharides

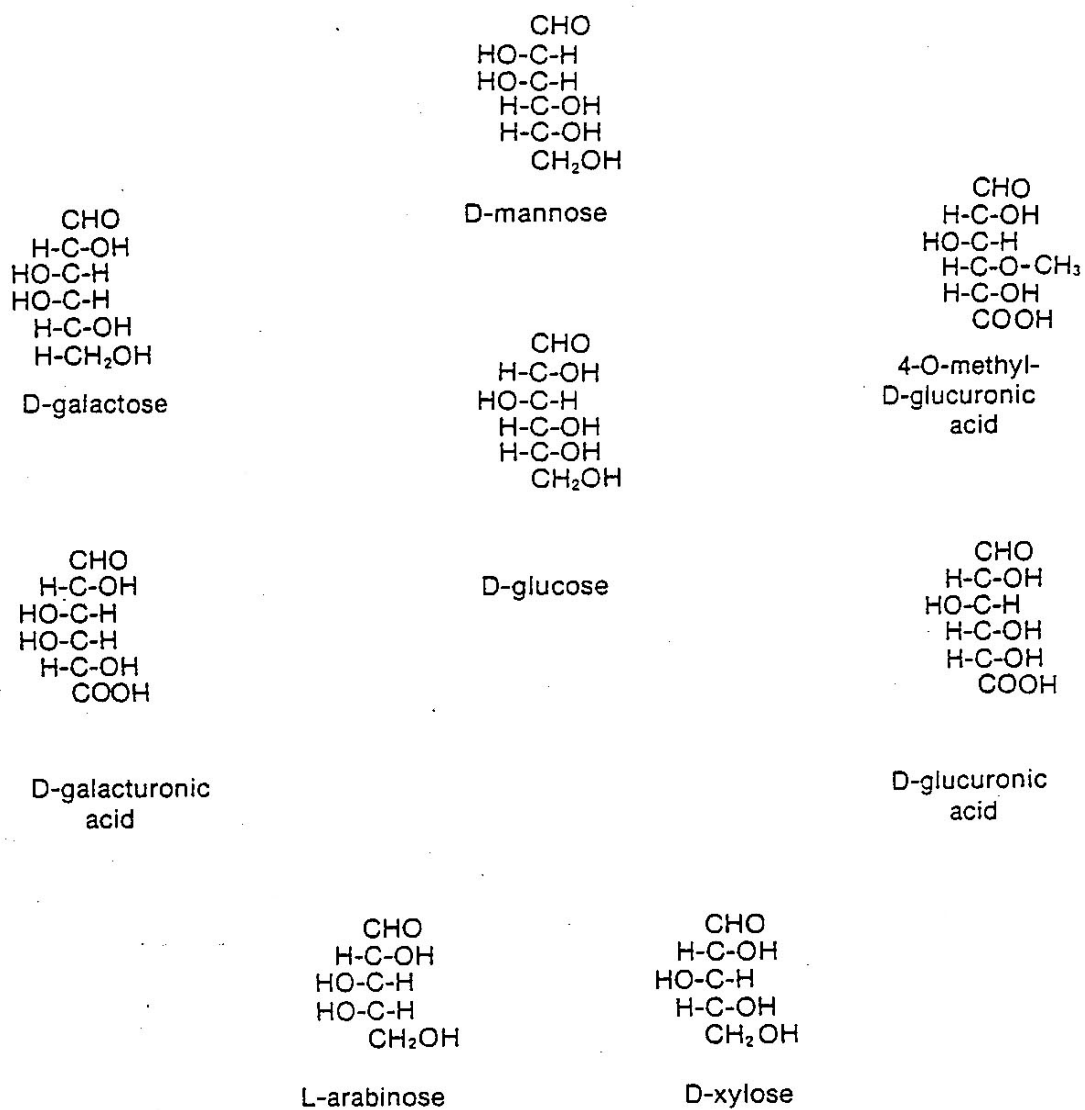


Figure 3-7: Structural Interrelationship of Commonly Occurring Hemicellulose Component Sugars

the hemicellulose polymers generally contain 50 units to 200 units and exhibit a branched rather than a linear structure.

These structural characteristics, as well as the number and proportion of different sugar residues present (degree of heteropolymerization), largely determine the observed physical properties of hemicelluloses. The heteropolymerization decreases the ability to form regular, tight-fitting crystalline regions and thus makes hemicellulose more soluble than cellulose. Solubility is also increased due to the branching, which decreases the number of intermolecular hydrogen bonds, and the decreased degree of polymerization compared to cellulose.

3.2.2.1 Xylans

Xylans, the most abundant of the hemicelluloses, are polymers of d-xylose ($C_5H_{10}O$). Xylose is a pentose sugar. The xylan fraction of cellulose is often termed pentosan. They are most abundant in agricultural residues such as grain hulls and corn stalks. Hardwoods (deciduous) and softwoods contain appreciable amounts of xylans. Xylan chains are short, exhibiting molecular weights on the order of 30,000 or less. In addition, some xylans contain carboxylic acid and methyl-ether groups. Typical xylans are shown in Fig. 3-8. The acidic xylans contain d-glucuronic acid or the methylester acid as terminal branch units.

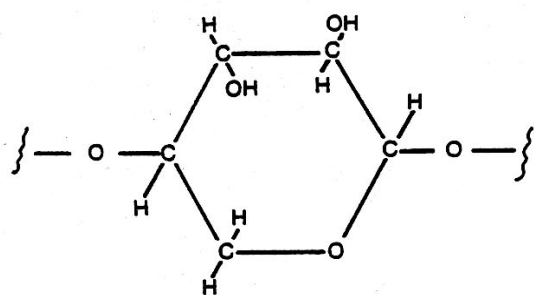
Some of the acid xylans are of low molecular weight. They are known as hemicellulose-B and are differentiated from the normal xylans and other neutral hemicelluloses in that they are not precipitated from the alkaline extract by neutralization.

3.2.2.2 Mannans

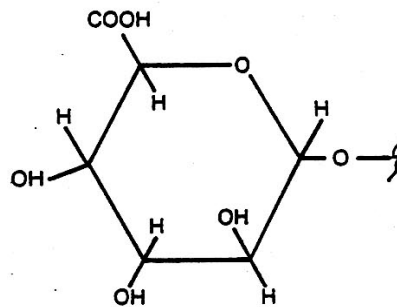
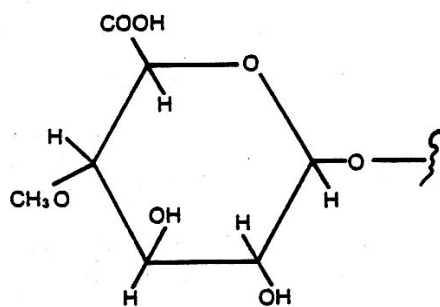
Mannan-based hemicelluloses include glucomannans, which are built up from linked d-glucose and d-mannose residues in about a 30:70 ratio, and galactoglucomannans, made up of linked d-galactose, d-glucose, and d-mannose in 2:10:30 ratios. In softwoods, mannans are present in substantial amounts while in hardwoods there is generally very little mannan hemicellulose.

3.2.3 Cellulose Data for Woods

Table 3-14 presents some data on the cellulose content of woods. The holocellulose fraction of hardwoods is composed principally of cellulose and xylans. The total content of mannans and other hemicelluloses averages only 4.8% for the four samples. In softwoods, the cellulose fraction is about the same as in hardwoods. However, mannans are present to a much greater extent; the mannans equal or exceed the total xylans in the conifers. Other hemicelluloses are present at 5.4% on the average for the four samples.



Xylan



Acid Xylans-Terminal Groups

Figure 3-8: Xylan Hemicellulose Structures

Table 3-14: Breakdown of Holocellulose Fraction of Woods ^a

	Wt% in Holocellulose				
	Cellulose	Xylans	Acidxylans	Mannans	Others
Hardwoods					
Trembling Aspen	71.5	20.0	4.1	2.9	1.5
Beech	64.5	23.8	6.5	2.9	2.3
Sugar Maple	69.8	20.0	5.9	3.1	1.2
Southern Red Oak	59.8	28.3	6.6	2.9	2.4
Softwoods					
Eastern hemlock	69.0	6.1	5.0	17.1	2.8
Douglas Fir	64.6	4.2	4.2	16.0	11.0
White spruce	65.2	9.5	5.0	16.3	3.9
Jack Pine	65.1	10.1	5.6	15.1	4.0

^aFrom Encyclopedia of Chem. Tech., 1963, p. 358.

3.2.4 Lignin

The noncarbohydrate component of the cell wall, termed lignin, is a three-dimensional polymer based primarily on the phenylpropane unit. Lignin is deposited in an amorphous state surrounding the cellulose fibers and is bound to the cellulose directly by ether bonds. Its exact structure is not known, although considerable information is available based on its chemical reactivity. In solubility analyses, lignin is defined as the cell wall portion not soluble in 72% sulfuric acid. Table 3-15 gives typical elemental analyses of wood lignins.

Table 3-15: Elemental Analysis of Wood Lignin

Type	C (%)	H (%)	O(%)	OCH ₃ (%)	Molecular Wt.
Softwood	63.8	6.3	29.9	15.8	10,000
Hardwood	59.8	6.4	33.7	21.4	5,000

It is assumed, based on much evidence, that the lignins are composed of several monomer groups as shown in Fig. 3-9. These are combined to form the polymer by a variety of linkages involving the aromatic rings and functional groups. The polymer formed contains only single aromatic rings as shown in 3-10 (structural formula).

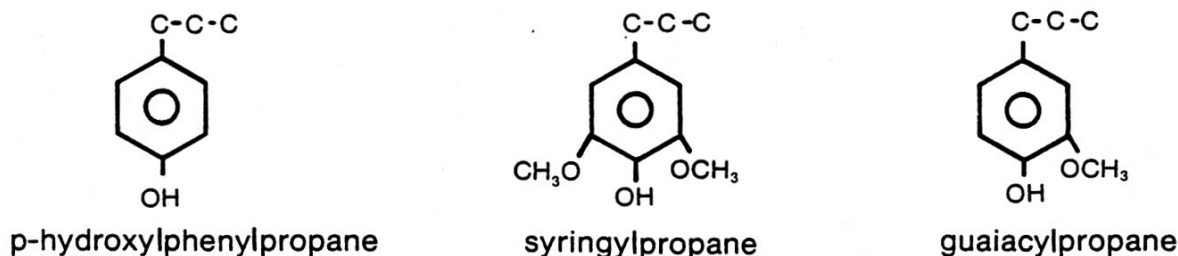


Figure 3-9: Several Monomer Units in Lignin

The representative structure contains the phenylpropane substituted as sinapyl, coniferyl, and p-coumaryl alcohols as shown in Fig. 3-11. Lignification, as discussed by Freudenberg (1965), is thought to occur by dehydration-polymerization of these alcohol units. Thermal pyrolysis of lignin generally yields a considerable amount of char. It is likely that thermal pyrolysis and lignification follow the same route to yield a condensed polynuclear aromatic structure.

The amount of lignin present varies among materials. Typical amounts for woods and barks are given in Tables 3-12 and 3-13. Table 3-16 gives data for a variety of other biomass materials.

Table 3-16: Lignin in Miscellaneous Plant Material ^a

Material	Wt %, Dry Unextracted Material
Rice hulls	40.0
Bagasse	20.3
Peanut shells	28.0
Pine needles	23.9
Wheat straw	13.9
Corncoobs	13.4

^a From Encyclopedia of Chem. Tech., 1963, p.361

3.2.5 Extractables

The nature and quantity of extractables vary widely among woods. Table 3-17 lists the type of extractables found in a variety of wood materials. The resins and volatile oils

are fragrant and found most commonly in softwoods. Waxes, fatty acids, pigments, and carbohydrates are commonly found in all woods. Starches account for about 3% of the total wood. Since the quality and nature of extractables vary, the products after pyrolysis and gasification vary.

Table 3-17: Extractable Components of Wood

<p>Volatile Oils (removed by steam of ether soluble)</p> <p>Terpenes ($C_{12}H_{16}$)</p> <p>Sesquiterpene ($C_{15}H_{24}$) and their oxygenated derivatives</p> <p>Resins and Fatty Acids (soluble in ether)</p> <p>Resin acids ($C_{20}H_{30}O_2$)</p> <p>Fatty acids (oleic, linoleic, palmitic)</p> <p>Glyceryl esters of fatty acids</p> <p>Waxes (esters of monohydroxyalcohols and fatty acids)</p> <p>Physterols (high molecular weight cyclic alcohols)</p> <p>Pigments (soluble in alcohol)</p> <p>Flavonols (multi-ring naphthenic and aromatic alcohols, chlorides, ketones acids)</p> <p>Pyrones (multi-ring naphthenic and aromatic alcohols, chlorides, ketones acids)</p> <p>Antranols (multi-ring naphthenic and aromatic alcohols, chlorides, ketones acids)</p> <p>Tannins (amorphous polyhydroxylic phenols)</p> <p>Carbohydrate Components (water soluble)</p> <p>Starch</p> <p>Simple sugars</p> <p>Organic acids</p>
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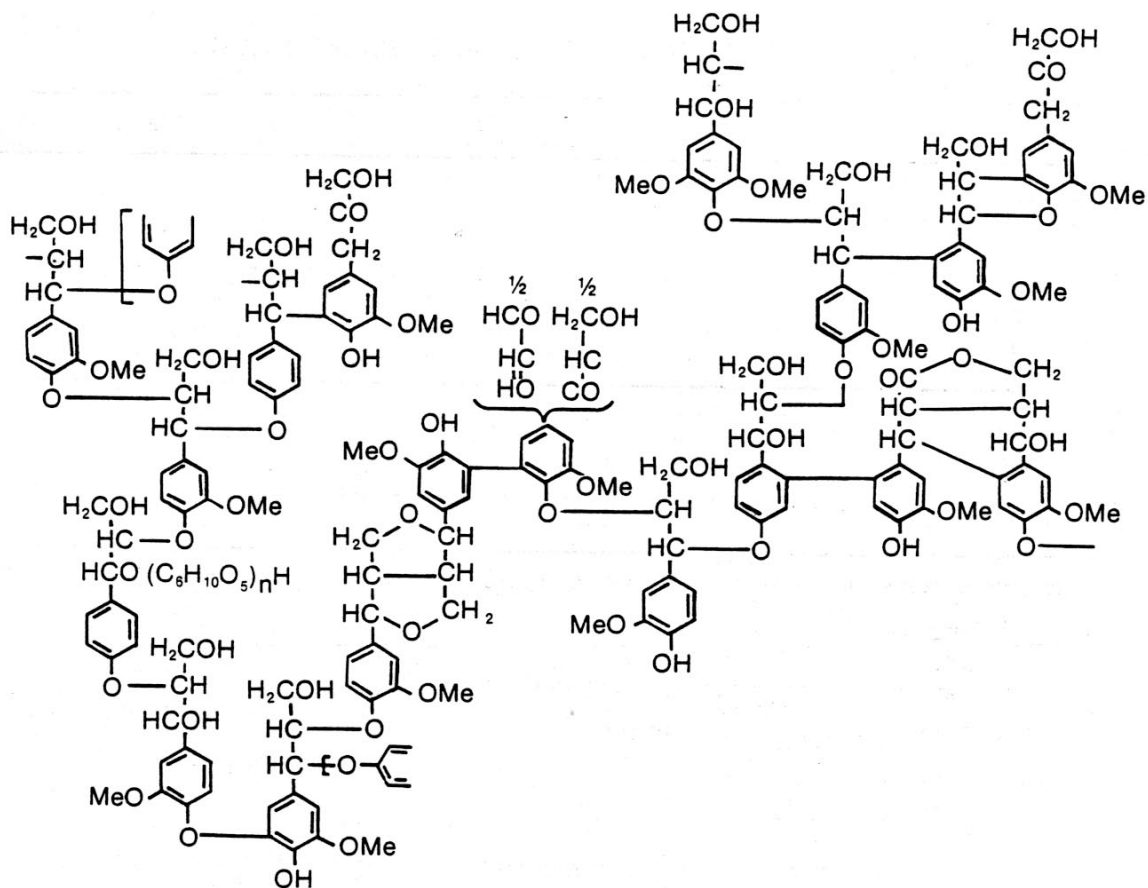


Figure 3-10: Representative Structure of Coniferous Lignin

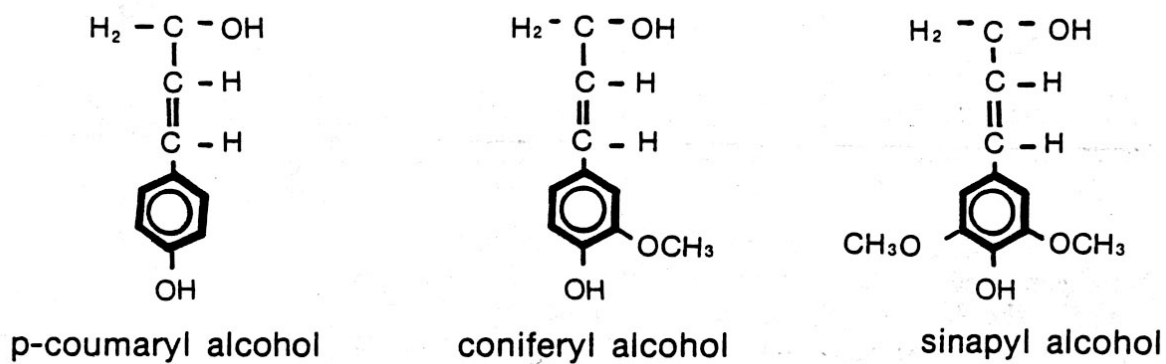


Figure 3-11: P-Hydroxycinnamyl Alcohols

Table 3-18 presents some typical extraction data on woods. The bulk of the extractables may be removed by hot water and ether. The ether-soluble portion is usually much greater for the softwoods, showing the higher content of volatile oils and resins. The hot water extraction, which leaches some tannins as well as the carbohydrates, gives yields approximately the same for the soft- and hardwoods.

Table 3-18: Extraction Data for Woods ^a

Sample	Wt % of Solubles	
	Hot Water	Ether
Softwoods		
Western yellow pine	5.05	8.52
Yellow cedar	3.11	2.55
Incense cedar	5.38	4.31
Redwood	9.86	1.07
Western white pine	4.49	4.26
Longleaf pine	7.15	6.32
Douglas fir	6.50	1.02
Western larch	12.59	0.81
White spruce	2.14	1.36
Hardwoods		
Tanbark oak	5.60	0.80
Mesquite	15.09	2.30
Hickory	5.57	0.63
Basswood	4.07	1.96
Yellow birch	3.97	0.60
Sugar Maple	4.36	0.25
Average—Softwoods	6.25	3.36
Average—Hardwoods	6.44	1.09

^aFrom Encyclopedia of Chem. Tech., 1963, p.358

3.3 WOOD STRUCTURE

Wood is composed of cells of various sizes and shapes. Long pointed cells are known as fibers; hardwood fibers are about 1mm in length, while softwood fibers vary in length from about 3mm to 8mm. The mechanical properties of wood depend largely on its density, which, in turn, is largely determined by the thickness of the cell walls.

3.3.1 Physical Structure of Softwoods

Figure 3-12 shows a typical softwood structure taken from Siau (1971). In softwoods, the fluid conducting elements are the longitudinal tracheids and ray tracheids. Longitudinal and horizontal resin canals are also present in many species.

Longitudinal tracheids, shown in Fig. 3-13, make up the bulk of the structure of softwoods. These are long, hollow, narrow cells having no openings that are tapered along the radial surfaces for a considerable portion of the lengths where they are in contact with other tracheids. The surfaces of the tracheids are dotted with pits, minute depressions in the plant tissue wall which permit the movement of water and dissolved materials between tracheids. The pit is covered with a semipermeable membrane. Pits are oriented in softwoods as adjacent pairs (pit pairs); fluid flow occurs between tracheids in the direction normal to the principal direction of flow.

The tracheid diameter varies from 15 to 80 μm according to species, with a length ranging from 1200 to 7500 μm . Average values of diameter and length, respectively, are 33 μm and 3500 μm . The inner diameter which is available for flow is typically 20-30 μm . The effective radius of the pit openings is 0.01 to 4 μm due to the restriction created by the membrane. Typically, a tracheid contains 50 pits. In addition to pit pairs allowing longitudinal flow, there are also pit pairs leading from longitudinal tracheids to ray tracheids, permitting radial flow.

The volumetric composition of a typical softwood is as follows:

Longitudinal tracheids	93%
Longitudinal resin canals	1%
Ray tracheids	6%

Since the principal voidage is oriented longitudinally, the magnitude of the permeability in the longitudinal direction is much greater than the radial permeability. Figure 3-14 shows a schematic model for flow through a softwood.

3.3.2 Physical Structure of Hardwoods

The structure of a typical hardwood is shown in Fig. 3-15. The dominant feature of the hardwood structure is the large open vessels or pores. Tracheids and pits are present but contribute significantly more resistance to flow. In a typical hardwood, the following structural composition is present:

Vessels	55%
Tracheids	26%
Woods rays	18%
Others	1%

Vessels are large, with diameters of 20 to 30 μm . The vessels are short, connected by “perforation plates” which offer very low flow resistance. Thus the vessels behave as long capillaries. Figure 3-16 shows the nature of flow through hardwoods.

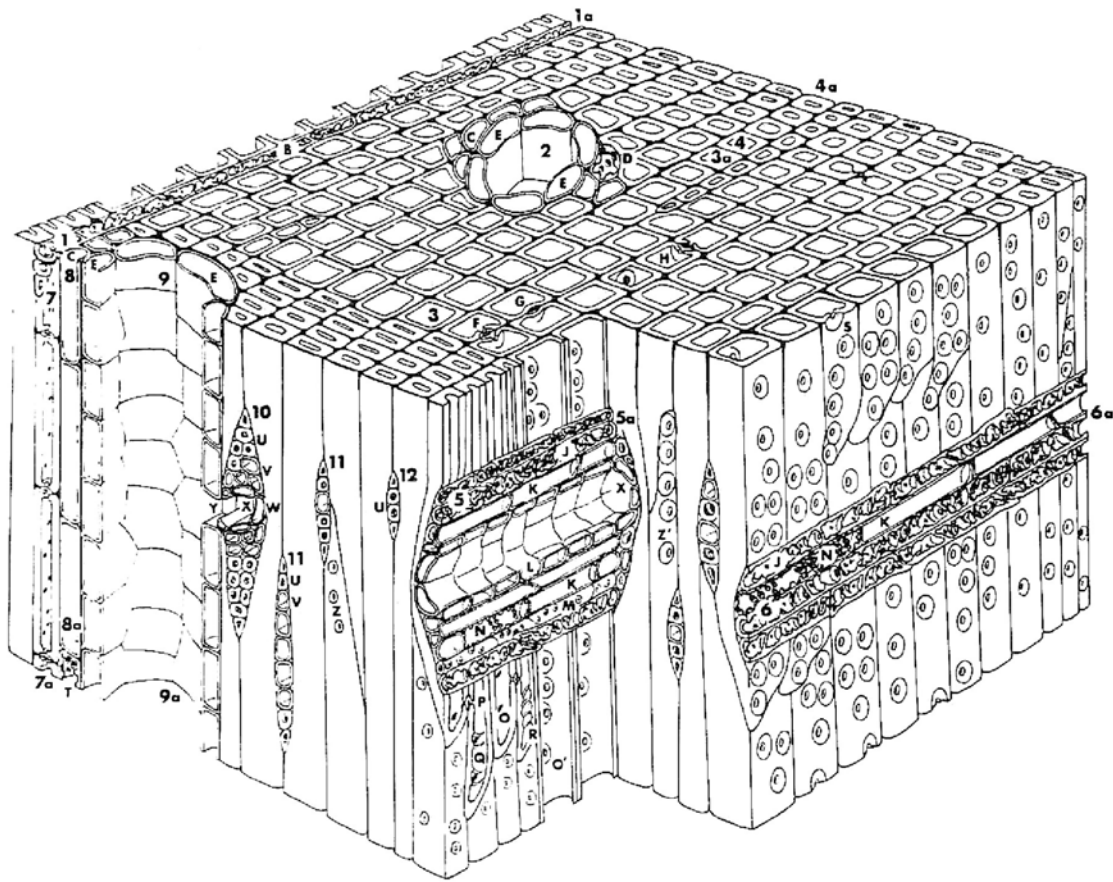


Figure 3-12: Gross Structure of a Typical Southern Pine Softwood

Transverse view: 1-1a, ray; B, dentate ray tracheid; 2, resin canal; C, thin-walled longitudinal parenchyma; D, thick-walled longitudinal parenchyma; E, epithelial cells; 3-3a, earlywood tracheids; F, radial bordered pit pair cut through torus and pit apertures; G, pit pair cut below pit apertures; H, tangential pit pair; 4-4a, latewood.

Radial view: 5-5a, sectioned fusiform ray; J, dentate ray tracheid; K, thin-walled parenchyma; L, epithelial cells; M, unsectioned ray tracheid; N, thick-walled parenchyma; O, latewood radial pit (inner aperture); O', earlywood radial pit (inner aperture); P, tangential bordered pit; Q, callitorid-like thickenings; R, spiral thickenings; S, radial bordered pits (the compound middle lamella has been stripped away removing crassulae and tori); 6-6a, sectioned uniseriate heterogenous ray.

Tangential view: 7-7a, strand tracheids; 8-8a, longitudinal parenchyma (thin-walled); T, thick-walled parenchyma; 9-9a, longitudinal resin canal; Y, opening between horizontal and vertical resin canals; 11, uniseriate homogeneous rays; 12, uniseriate homogeneous ray; Z, small tangential pits in latewood; Z', large tangential pits in earlywood.

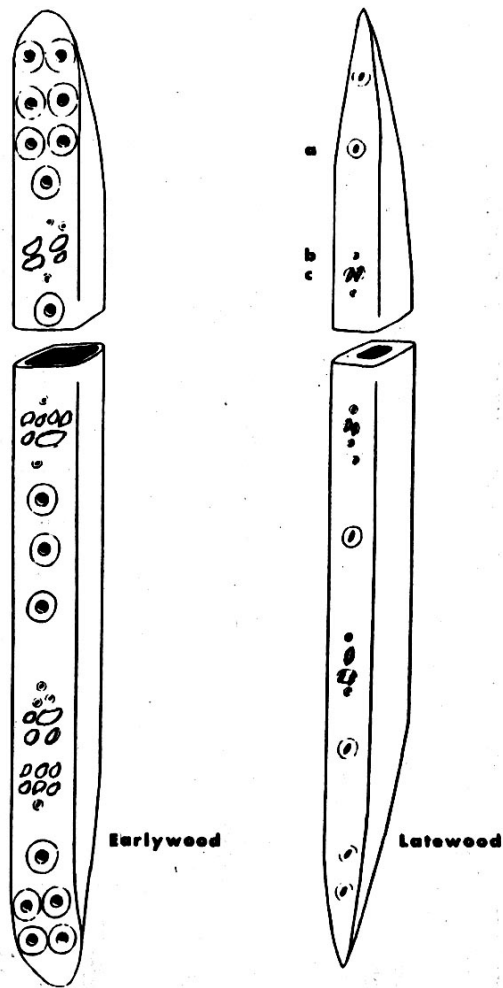


Figure 3-13: Radial Surfaces of Earlywood and Latewood Tracheids

(a) intertracheal bordered pits; (b) bordered pits to tracheids; (c) pinoid pits to ray parenchyma

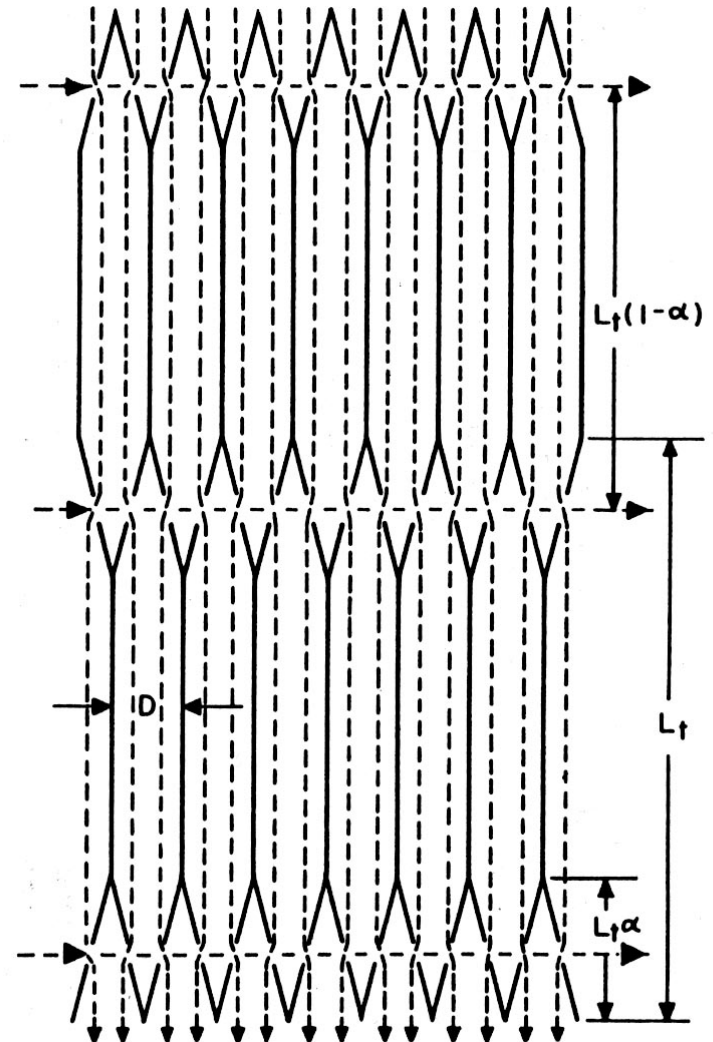


Figure 3-14: Softwood Flow Model

Tangential section showing pits on the radial surfaces of the tapered ends of the tracheids

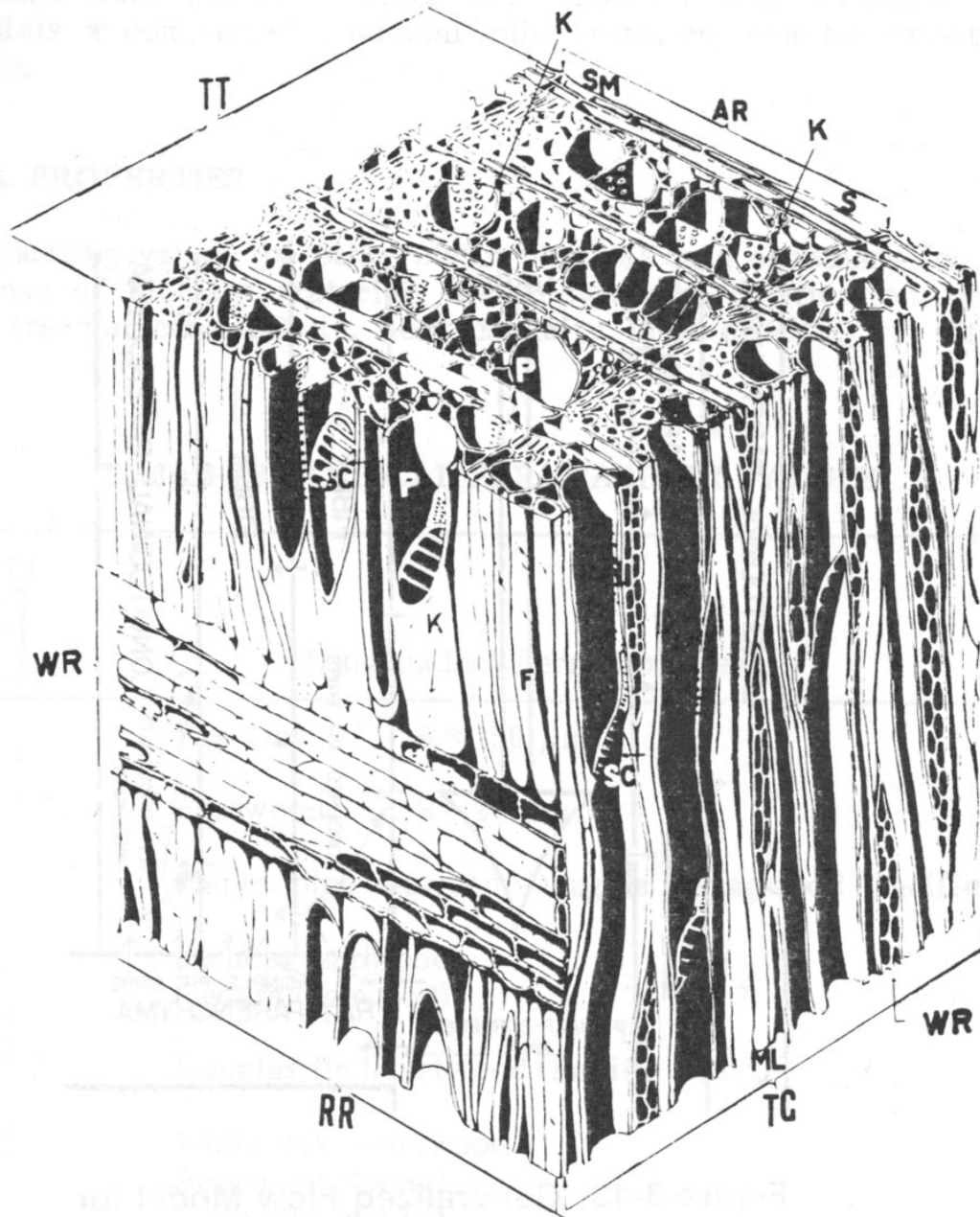


Figure 3-15: Gross Structure of a Typical Hardwood

Plane TT is the cross section, RR is the radial surface, and TG is the tangential surface. The vessels or pores are indicated by P, and the elements are separated by scalariform perforation plates, SC. The fibers, F, have small cavities and thick walls. Pits in the walls of the fibers and vessels, K, provide for the flow of liquid between the cells. The wood rays are indicated at WR. AR indicates one annual ring. The earlywood (springwood) is designated S, while the latewood (summerwood) is SM. The true middle lamella is located at ML.

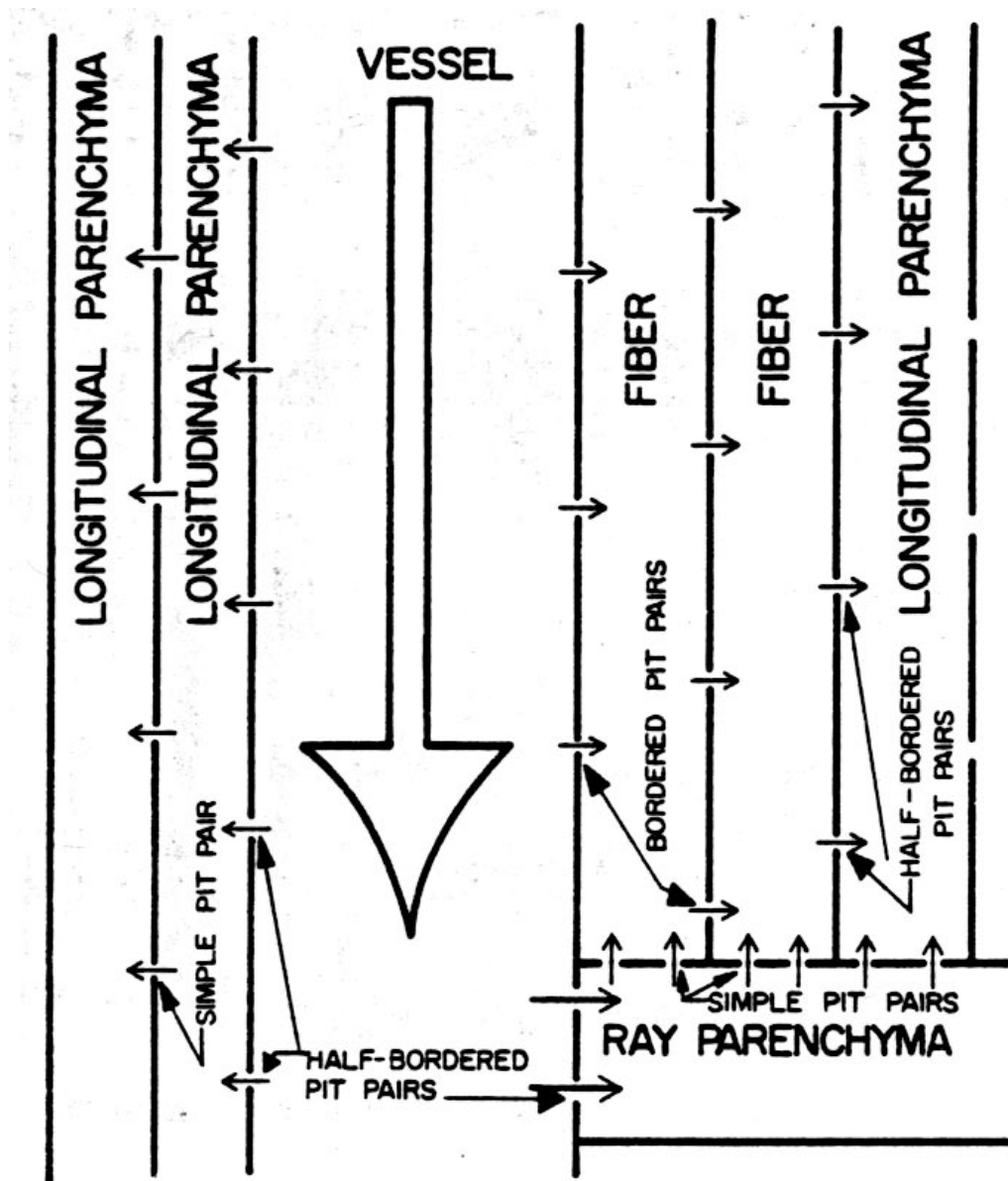


Figure 3-16: Generalized Flow Model for Hardwoods

3.3.3 Permeability

Permeability is important in pyrolysis. During heating, pyrolysis gases and liquids are generated within the particle and must pass through the porous structure to the surroundings. Low permeability may significantly affect the product distribution by increasing the residence time of the primary pyrolysis products in the hot zone, thereby increasing the probability that they will enter into secondary reactions. Pelletized, densified biomass will have a low permeability compared with natural woods. Table 3-19 shows the range of permeability for various natural woods.

In natural soft- and hardwood structures, it is evident that the porosity is directed principally in the vertical direction in the livewood. Physical properties such as thermal conductivity and diffusivity therefore depend on direction within fresh wood. Such a behavior is termed anisotropic (aeolotropic).

Table 3-19: Typical Permeability Values

Permeability (cm ³ (air)cm ⁻¹ atm ⁻¹)	Longitudinal Permeabilities	
10 ⁴	Red Oak	R ≈ 150 μm
10 ³	Basswood	R ≈ 20 μm
10 ²	Maple, oine sapwood, Douglas fir sapwood (Pacific Coast)	
10 ¹	Spruces (sapwood), cedars (sapwood)	
10 ⁰	Douglas fir heartwood (Pacific Coast)	
10 ⁻¹	White oak heartwood, Beech heartwood, Cedar heartwood	
	Douglas fir heartwood (intermountain)	
10 ⁻²	}	Transverse permeabilities. (The species are in approximately the same order as for longitudinal permeabilities)
10 ⁻³		
10 ⁻⁴		

3.4 PHYSICAL PROPERTIES

In addition to heating value, the other major physical data necessary for predicting the thermal response of biomass materials under pyrolysis, gasification, and combustion processes are thermal conductivity, heat capacity, true density, and diffusion coefficients.

3.4.1 Thermal Conductivity

Thermal conductivity is defined in general terms as a proportionality factor which relates heat flow through a material to a temperature difference across a specified distance in that material. Mathematically, thermal conductivity is defined by Fourier's Law of Heat Conduction, given here for unidimensional heat flux in the x-direction in rectangular coordinates:

$$q_x = -k_x \frac{dT}{dx} \quad (3-23)$$

Most homogeneous materials are isotropic, and the thermal conductivity varies only with temperature

$$q = -k \nabla T \quad (3-24)$$

However, most naturally occurring biomass materials are anisotropic. For wood, the thermal conductivity is a function of temperature and spatial direction. Modified biomass materials, such as densified wood, probably do not exhibit the same type of anisotropic behavior as the naturally occurring biomass materials. Thermal conductivity should be related to the various materials present in a substance. Thus in biomass thermal conductivity should be a function of the major constituents, including moisture, cellulose, hemicellulose, and lignin.

Table 3-20 compiles available thermal conductivity data for biomass materials. No data are available for compacted biomass feedstocks. In general, no chemical analyses are presented with the data. The bulk of the data are probably effective thermal conductivities of powders rather than of the solids. The conductivities for solid woods, for example, are two to ten times greater than for many of the other biomass materials listed in Table 3-20 (e.g., sawdust and redwood shavings). Most data sources do not specify the state of the materials.

Steinhagen (1977) has summarized thermal conductivity data for several woods over the range -40° C to +100° C as a function of moisture content and has shown that moisture is an important parameter in wood conductivity. Since the moisture content is not known for the bulk of the entries in Table 3-20, the data presented are at best only semi-quantitative.

Completely lacking in the available data are thermal conductivities at higher temperatures. This is primarily because the majority of the data were determined by researchers in the forest products industry interested in the thermal properties of wood and insulating materials for home heating and cooling applications. If thermal conductivity values are to be used in modeling pyrolysis or gasification processes, then new data over the actual range of processing conditions must be developed, including data for densified materials.

Table 3-20: Thermal Conductivity of Selected Biomass Materials

Material	Bulk Density (lb/ft³)	Temperature (°F)	Thermal Conductivity (Btu/ft-h-°F)	Reference
Ashes, wood	--	32 - 212	0.040	Kern 1950
Cardboard	--	--	0.037	Kern 1950
Carbon, porous, with grain				
Grade 60 48% porosity	65.5 ^a	Room Temp.	0.083	Perry and Chilton 1973
Grade 45 47% porosity	64.9	Room Temp.	0.083	Perry and Chilton 1973
Grade 25 47% porosity		Room Temp.	0.083	Perry and Chilton 1973
Carbon Refractory brick - 17% porosity		Room Temp.	1.33	Perry and Chilton 1973
Celotex, sheet fiber from sugar cane	13.2	--	0.028	Handbook Chem. Phys, 1966
	14.8	--	0.028	Handbook Chem. Phys, 1966
	14.4	32	0.0253	McAdams 1954
	14.4	0	0.0242	McAdams 1954
	14.4	-100	0.0208	McAdams 1954
	14.4	-200	0.0175	McAdams 1954
	14.4	-300	0.0133	McAdams 1954
Charcoal - from maple, beech, birch				
Coarse	13.2	--	0.030	Handbook Chem. Phys, 1966
6 mesh	15.2	--	0.031	Handbook Chem. Phys, 1966
20 mesh	19.2	--	0.032	Handbook Chem. Phys, 1966
Charcoal flakes	11.9	176	0.043	McAdams 1954

Material	Bulk Density (lb/ft ³)	Temperature (°F)	Thermal Conductivity (Btu/ft-h-°F)	Reference
	15	176	0.051	McAdams 1954
	--	0 to 100	0.0133	Handbook Chem. Phys, 1966
Cork, regranulated				
Fine particles	9.4	--	0.025	Handbook Chem. Phys, 1966
1/16-in. Particles	8.1	--	0.026	Handbook Chem. Phys, 1966
Corkboard	5.4	--	0.021	Handbook Chem. Phys, 1966
	7.0	--	0.022	Handbook Chem. Phys, 1966
	10.6	--	0.025	Handbook Chem. Phys, 1966
	14.0	--	0.028	Handbook Chem. Phys, 1966
	6.9	32	0.0205	McAdams 1954
	6.9	0	0.0200	McAdams 1954
	6.9	-100	0.0183	McAdams 1954
	6.9	-200	0.0142	McAdams 1954
	6.9	-300	0.0100	McAdams 1954
Cork, pulverized	10.0	32	0.035	McAdams 1954
	10.0	100	0.039	McAdams 1954
	10.0	200	0.032	McAdams 1954
Cotton	5.0	200	0.037	McAdams 1954
	5.0	100	0.035	McAdams 1954
	5.0	32	0.0325	McAdams 1954
	5.0	-100	0.0276	McAdams 1954

Material	Bulk Density (lb/ft ³)	Temperature (°F)	Thermal Conductivity (Btu/ft-h-°F)	Reference
	5.0	-200	0.0235	McAdams 1954
Cotton	5.0	-300	0.0198	McAdams 1954
Graphite - 2 3/4" Dia., 3/4 " Thick, 30% porosity	98.6 ^a	--	7.33	Handbook Chem. Phys, 1966
Porous, Grade 60 52% porosity	65.5 ^a	--	4.17	Handbook Chem. Phys, 1966
Porous, Grade 45 53% porosity	64.9 ^a	--	3.75	Handbook Chem. Phys, 1966
Porous, Grade 25 53% porosity	64.3 ^a	--	3.33	Handbook Chem. Phys, 1966
Paper	--	--	0.075	McAdams 1954
Paper or pulp, macerated	2.5-3.5	--	0.0121	Lewis 1968
Sawdust, various	12.0	--	0.034	Handbook Chem. Phys, 1966
Redwood	10.9	--	0.035	Handbook Chem. Phys, 1966
(and shavings)	8-15	--	0.0375	Handbook Chem. Phys, 1966
Sawdust (soft pine and oak)				
10 - 40 mesh	--	-295	0.016	Chow 1948
	--	-180	0.0195	Chow 1948
		-105	0.0235	Chow 1948
		-55	0.0265	Chow 1948
		-20	0.0295	Chow 1948
		5	0.0325	Chow 1948
		30	0.0355	Chow 1948
		35	0.0385	Chow 1948
		62	0.040	Chow 1948

Material	Bulk Density (lb/ft ³)	Temperature (°F)	Thermal Conductivity (Btu/ft-h-°F)	Reference
^a Apparent density, defined in Section 3.4.3				
Shredded redwood bark	4.0	32	0.0290	McAdams 1954
	4.0	-100	0.0235	McAdams 1954
	4.0	-200	0.0196	McAdams 1954
	4.0	-300	0.0155	McAdams 1954
	--	-50	0.0168	Rowley et al. 1945
	--	-25	0.0180	Rowley et al. 1945
	--	25	0.0203	Rowley et al. 1945
	--	75	0.0226	Rowley et al. 1945
Sheet insulite, from wood pulp	16.2	--	0.028	Handbook Chem. Phys, 1966
	16.9	--	0.028	Handbook Chem. Phys, 1966
Wood fiber, mat	1.7	-50	0.016	Rowley et al. 1945
	1.7	0	0.018	Rowley et al. 1945
	1.7	50	0.020	Rowley et al. 1945
	1.7	100	0.023	Rowley et al. 1945
Wood fiber, blanket	3.5	-50	0.016	Rowley et al. 1945
	3.5	0	0.018	Rowley et al. 1945
	3.5	50	0.020	Rowley et al. 1945
	3.5	100	0.022	Rowley et al. 1945
Wood fiber, excelsier	1.64	-50	0.019	Rowley et al. 1945
	1.64	0	0.022	Rowley et al. 1945

Material	Bulk Density (lb/ft ³)	Temperature (°F)	Thermal Conductivity (Btu/ft-h-°F)	Reference
	1.64	50	0.022	Rowley et al. 1945
Wood fiber, excelsier	1.64	100	0.024	Rowley et al. 1945
Solid woods				
Balsa	8 - 12	-300	0.0151	Gray et al. 1960
	8 - 12	-285	0.0150	Gray et al. 1960
	8 - 12	-260	0.0167	Gray et al. 1960
	8 - 12	-207	0.0183	Gray et al. 1960
	8 - 12	-190	0.0192	Gray et al. 1960
	8 - 12	-160	0.0233	Gray et al. 1960
	8 - 12	-130	0.0233	Gray et al. 1960
	8 - 12	-95	0.0232	Gray et al. 1960
Balsa, across grain	7.3	--	0.028	Handbook Chem. Phys, 1966
	8.8	--	0.032	Handbook Chem. Phys, 1966
	20	--	0.048	Handbook Chem. Phys, 1966
Cypress, across grain	29	--	0.056	Handbook Chem. Phys, 1966
Mahogany, across grain	34	--	0.075	Handbook Chem. Phys, 1966
Maple, across grain	44.7	122	0.11	McAdams 1954
Fir	26	75	0.063	Chapman 1974
Oak	30 - 38	86	0.096	Chapman 1974
Yellow pine	40	75	0.065	Chapman 1974
White pine	27	86	0.087	Chapman 1974

Material	Bulk Density (lb/ft ³)	Temperature (°F)	Thermal Conductivity (Btu/ft-h-°F)	Reference
Pine, white, across grain	34	59	0.087	McAdams 1954
	32	--	0.032	Handbook Chem. Phys, 1966
Pine, Virginia, across grain	34	--	0.082	Handbook Chem. Phys, 1966
Pine board, 1 ¼" thick	--	-50	0.0515	Gray et al. 1960
	--	0	0.054	Gray et al. 1960
	--	50	0.0575	Gray et al. 1960
	--	100	0.059	Gray et al. 1960
Pine, with grain	34.4	59	0.20	McAdams 1954
Oak, across grain	51.5	59	0.12	McAdams 1954

Equations have been developed for wood, expressing thermal conductivity as a function of of moisture and specific gravity for combined heat flow in the radial and tangential directions (McLean 1941). The expression was derived at ambient temperatures.

For moisture contents less than 40% the thermal conductivity is expressed as

$$k = S(0.116 + 0.00233M) + 0.01375 \quad (3-25)$$

and for moisture contents greater than 40%

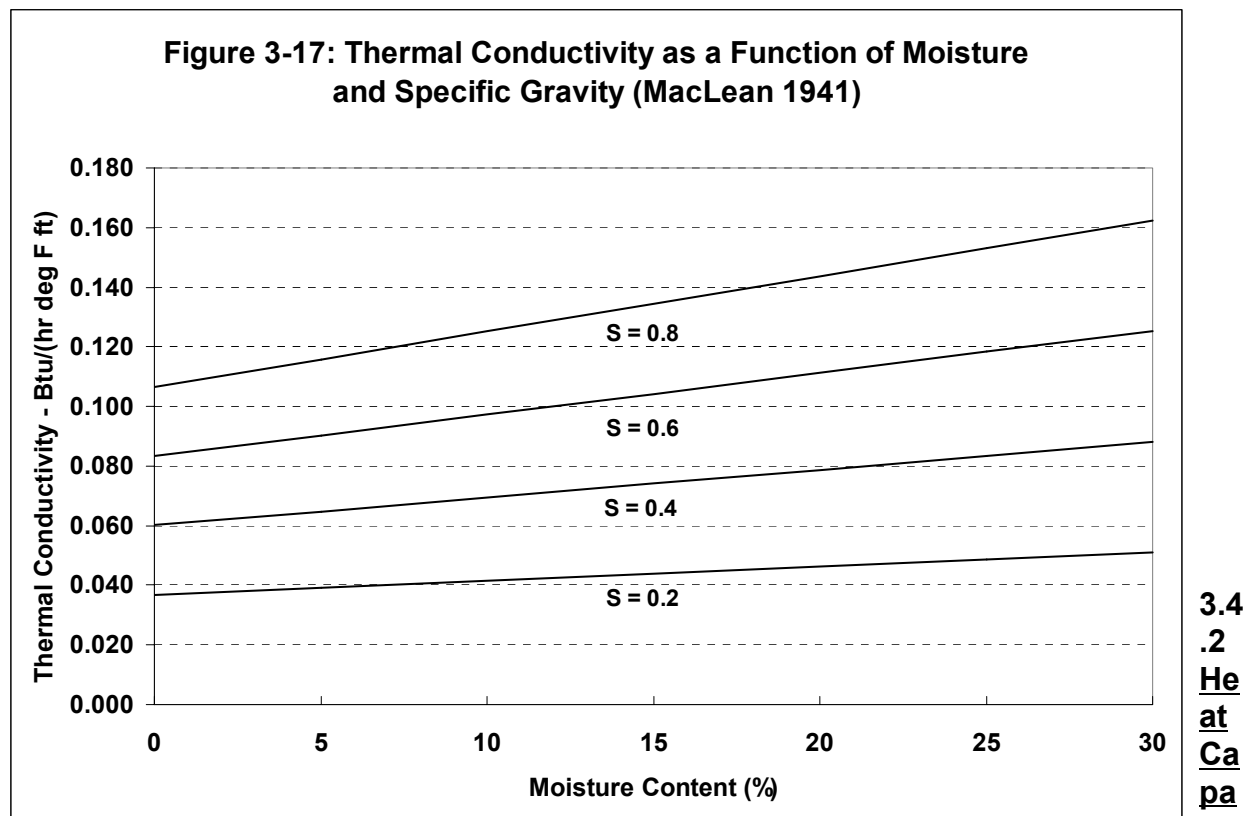
$$k = S(0.116 + 0.00317M) + 0.01375 \quad (3-26)$$

where S = apparent specific gravity, as defined in Section 3.4.3
 M = Percent moisture content, oven dry basis, or

$$M = 100(W - D)/D, \quad (3-27)$$

where W = Original weight
 D = Dry weight after oven drying

A plot of thermal conductivity as a function of moisture content and specific gravity using equation 3-25 is given in Figure 3-17.



city

Heat capacity, as normally reported, is defined in terms of the enthalpy content of a material and represents the relative ability of a material to store energy. Enthalpy is a function of temperature and pressure.

$$H = H(T,P) \quad (3-28)$$

and

$$dH = (\partial H/\partial T)_P dT + (\partial H/\partial P)_T dP \quad (3-29)$$

For solids and liquids $\partial H/\partial P$ is very small and

$$dH = (\partial h/\partial T)_P dT \quad (3-30)$$

By definition the temperature dependency term $(\partial H/\partial P)_P$ is called heat capacity at constant pressure, C_p , and is reported on a per unit weight basis. The resulting equation for the enthalpy change is as follows:

$$\Delta H = \int_{T_O}^T C_p dT \quad (3-31)$$

This equation is normally used for materials of constant mass and no phase transitions. For example, if water is driven out of wood the apparent heat capacity may change very rapidly with temperature; the same is true for other phase transitions. Generally, if phase transitions are incorporated the enthalpy change will be:

$$\Delta H = \int_{T_O}^{T_P} C_p^a dT + \Delta H_{\text{PHASE CHANGE}} + \int_{T_P}^T C_p^b dT \quad (3-32)$$

where

C_p^a, C_p^b = heat capacities of phases 1 and 2

T_P = temperature at which phase change occurs

The heat capacity is a function of the composition and temperature but not the density of the material as long as compacting does not alter the chemical structure.

The data on heat capacity are limited. Some typical values are given in Table 3-21. No characterization data are reported for the samples.

Several C_p equations have been developed to predict the heat capacities of wood at temperatures to 100 °C. As an example of specific heat equations for woods, Beall (1968) shows the equation in which moisture is an important parameter in estimating the heat capacity:

$$C_p = 0.259 + (9.75 \times 10^{-4})M + 6.05 \times 10^{-4}T_1 + 1.3 \times 10^{-5}MT_1, \quad (3-33)$$

where

M = % moisture, up to 27%.

Table 3-21: Heat Capacity

Material	Temperature (°F)	Heat capacity (Btu lb ⁻¹ °F ⁻¹)	Reference
Carbon	78-168	0.168	Perry 1973
	103-1640	0.314	Perry 1973
	132-2640	0.387	Perry 1973
Charcoal	50	0.16	Perry 1973
Cellulose	--	0.32	Perry 1973
Oak	--	0.57	Perry 1973
Fir	75	0.65	Chapman 1974
Yellow pine	75	0.67	Chapman 1974
Cork	68	0.45	Chapman 1974

Other methods are available and generally are for the same temperature range.

As with thermal conductivity, no references were readily available for heat capacity of biomass materials for the temperature range of thermal processing conditions needed for pyrolysis or gasification; new data are needed for applicable temperature ranges.

3.4.3 Density

The density of the material is important in considering energy contents of fuels on a volumetric basis, such as for transporting, solids handling, and sizing reaction vessels. There are three ways of reporting solid material density: bulk density, apparent particle

density, and skeletal density. These density values differ in the way in which the material volume is calculated. The bulk density volume basis includes the actual volume of the solid, the pore volume, and the void volume between solid particles. Apparent particle density includes solid volume and pore volume. Skeletal density, or true density, includes only solid volume. The three values are related as follows:

$$\rho_a = \rho_s(1-\epsilon_p) \quad (3-34)$$

$$\rho_b = \rho_a(1-\epsilon_b), \quad (3-35)$$

where

ρ_s = skeletal density, weight/volume

ρ_a = apparent density, weight/volume

ρ_b = bulk density, weight/volume

$$\epsilon_p = \text{particle porosity} = \frac{\text{Volume of pores}}{\text{Volume of pores and volume of solid}}$$

$$\epsilon_b = \text{bed porosity} = \frac{\text{Volume of external voids}}{\text{Volume of external voids and volume of particles}}$$

Densification of biomass is accomplished by reducing the particle porosity ϵ_p .

The density of biomass depends on the nature of the material, its moisture content, and degree of densification. Raw, over-dry biomass (with 7% to 8% moisture) has an apparent density of about 40 lb/ft³ (hardwoods) and 28 lb/ft³ (softwoods). The density of woods with high moisture contents can be as high as 60 lb/ft³. Densification produces particles with apparent bone dry densities of 55 lb/ft³ to 75 lb/ft³. The skeletal density of over dry biomass has been reported to be 91 lb/ft³ (Siau 1971). Bulk densities of a number of biomass materials are given in Table 3-20. Apparent densities of a number of biomass materials are given in Table 3-22.

3.4.3.1 Effect of Moisture Content on Density

The apparent density of wood and biomass depends on the moisture content. The dry and wet biomass apparent densities are related as follows from the moisture content obtained from the proximate analysis of the raw feedstock:

$$\rho_a(D) = (1-M) \rho_a(R), \quad (3-36)$$

where

$\rho_a(D)$ = apparent density of dry biomass,

$\rho_a(R)$ = apparent density of raw biomass, and

M = proximate moisture.

For a typical raw biomass with 50% moisture and apparent dry density of 30 lb/ft^3 , the raw biomass sample has a density of 60 lb/ft^3 .

Table 3-22: Apparent Density of Selected Woods
(Jenkins, 1989)

Wood Type	Specific Gravity	Density (lb/ft ³)
Almond	0.78	48.67
Alder (red)	0.38	23.71
Ash (white)	0.54	33.70
Aspen	0.36	22.46
Bald cypress	0.43	26.83
Beech	0.57	35.57
Birch, yellow	0.55	34.32
Cedar, incense	0.35	21.84
Cottonwood	0.37	23.09
Elm, American	0.46	28.70
Fir, balsam	0.32	19.97
Hemlock, mountain	0.42	26.21
Hickory, pecan	0.61	38.06
Maple, sugar	0.57	35.57
Oak, northern red	0.56	34.94
Oak, white	0.60	37.44
Pine, jack	0.40	24.96
lodgepole	0.39	24.34
ponderosa	0.39	24.34
sugar	0.34	21.22
Poplar, balsam	0.30	18.72
Redwood, old growth	0.39	24.34
Spruce, black	0.38	23.71
Tanoak	0.58	36.19
Yellow poplar	0.40	24.96

3.4.3.2 Densification

Densification by compaction reduces the internal voidage of the biomass material and reshapes the particles so that the bulk density is increased. The bulk density of green wood chips is typically 20 lb/ft³, while the apparent density is on the order of 60 lb/ft³. The typical external void fraction, ϵ_b , for chips is therefore about 0.67. The high voidage is due to the shape of the particles. Reshaping the particles to cylinders typically reduces the void fraction ϵ_b to about 0.5 and thus raises the bulk density to about 30 lb/ft³. Thus the weight per unit volume is increased 50% by reshaping, and more material can be transported in the same carrier volume.

Densification of biomass by decreasing the particle porosity further improves handling. For raw, dry biomass of apparent density of 30 lb/ft³, the particle porosity, ϵ_p , is typically 0.67 assuming 91 lb/ft³ for the skeletal density. For densified samples, with reported apparent bone dry densities of 55 lb/ft³ to 75 lb/ft³, the particle porosity has decreased to 0.4 to 0.18. Thus in densification a large fraction of the internal voidage is removed.

3.4.4 Diffusion Coefficients in Biomass Materials

No data are readily available in the literature on gas diffusion coefficients in either natural or pelleted biomass materials or in the pyrolysis chars.

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